



Waste management strategy for EU DEMO: status, challenges and perspectives

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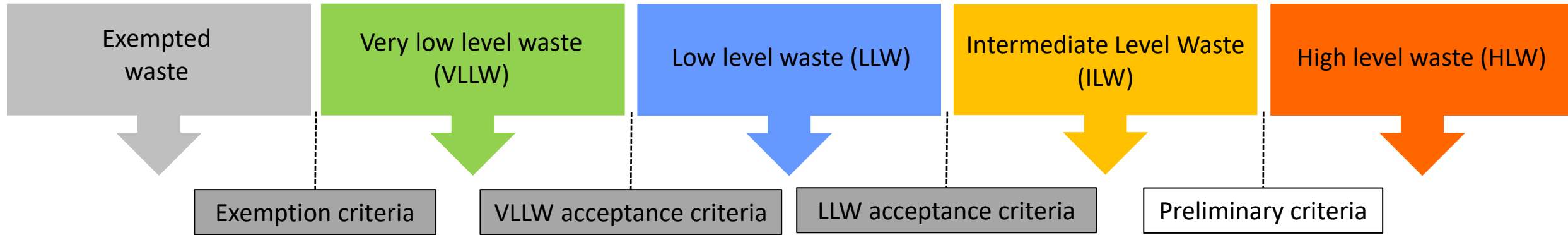
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- Introduction
- Waste classification status
- Challenges
 - Reduction of the radiotoxicity
 - Reduction of the radioactive waste amounts
- Perspectives for EU DEMO
- Conclusions

- European DEMO objectives
 - Net electricity, closed-tritium fuel cycle and plant availability
 - While demonstrating the **safety and environmental advantages of fusion power compared with fission designs**
- **Coherent strategy** for dealing with the waste needs to be part of the **justification for realizing DEMO**:
 - Minimization of the amount of radioactive waste produced
 - Minimization of the long-term geological disposal waste
 - Ability to detritiate efficiently
- No Host country, so no regulatory framework but shall be **part of the design process**

Waste classification status

Waste classification status



Focus on long-term geological waste disposal

LLWR (UK) Waste Acceptance Criteria:

- Total beta/gamma limit $< 1.2 \times 10^4$ Bq/g
- Total alpha $< 4 \times 10^3$ Bq/g

CSA (FR) Waste Acceptance Criteria

- Total alpha $< 4 \times 10^3$ Bq/g
- $^3\text{H} < 2 \times 10^5$ Bq/g
- $^{14}\text{C} < 9.2 \times 10^4$ Bq/g
- $^{60}\text{Co} < 1.3 \times 10^8$ Bq/g
- $^{59}\text{Ni} < 1.1 \times 10^5$ Bq/g
- $^{63}\text{Ni} < 3.2 \times 10^6$ Bq/g
- $^{94}\text{Nb} < 1.2 \times 10^2$ Bq/g
- $^{93}\text{Mo} < 3.8 \times 10^4$ Bq/g

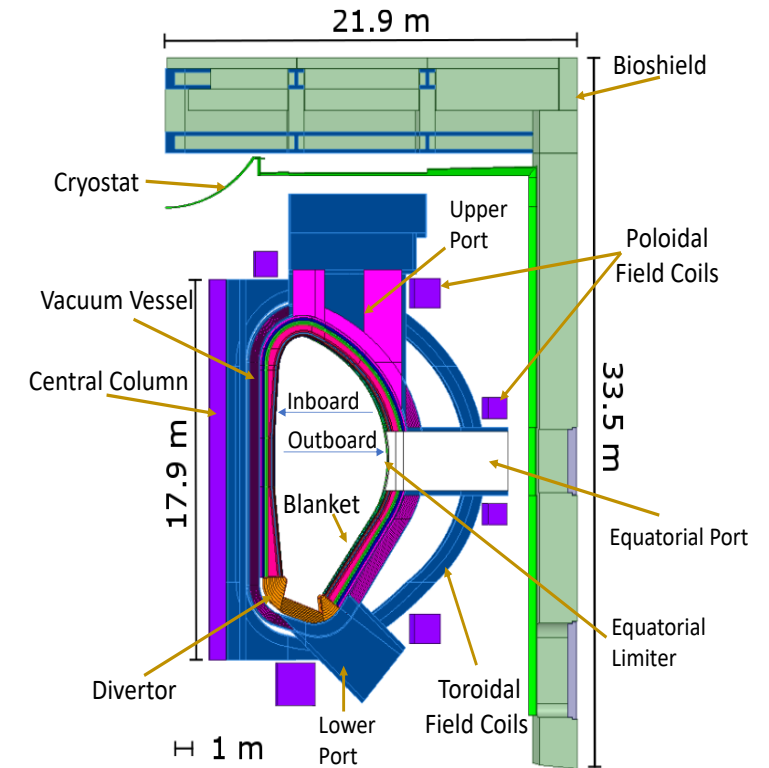
Decay heat limit within the disposal box:

- UK limits: 60 W for 2 m box or 2 W/t of waste,
- FR limits: 10 W/package or 2.5 W/t (considering a packing factor of 5t per 5 m³ package for massive components)

Waste classification status

- Classification of WCLL and HCPB concepts
- End-of-life for ex-vessel component (70 dpa), 20 dpa irradiation damage in BB First Wall, 0.5 dpa in target Cu of divertor

Water-cooled lithium lead (WCLL)	
Structural material	EUROFER97
First wall	W
Tritium breeder	
Neutron multiplier	Pb-15.7%Li
Helium-cooled pebble bed (HCPB)	
Structural material	EUROFER97
First wall	W
Tritium breeder	Advanced ceramic breeder pebbles ($\text{Li}_4\text{SiO}_4 + 35\% \text{mol Li}_2\text{TiO}_3$) KALOS (KARlsruhe Lithium OrthoSilicate)
Neutron multiplier	Be_{12}Ti hexagonal prismatic blocks



Identify the nuclides responsible for the classification
 Determine if changes in the design could improve the waste performance

Waste classification status – HLW assessment



WCLL Components		Dominant nuclides	
		Above 2 W/t of waste	
		at 1 year	at 50 years
Blanket (detritiation 99%)	Inboard	⁵⁴ Mn (53%), ⁵⁵ Fe (6%), ⁶⁰ Co (11%), ¹⁸² Ta (25%), ¹⁸¹ W (1%), ¹⁸⁵ W (2%)	
	Outboard	⁵⁴ Mn (59%), ⁵⁵ Fe (7%), ⁶⁰ Co (9%), ¹⁸² Ta (21%), ¹⁸¹ W (1%), ¹⁸⁵ W (2%)	
Limiter		⁵⁴ Mn (19%), ⁶⁰ Co (30%), ¹⁸² Ta (30%), ¹⁸¹ W (8%), ¹⁸⁵ W (9%)	
Divertor		⁵⁴ Mn (31%), ⁵⁵ Fe (4%), ⁶⁰ Co (33%), ¹⁸² Ta (25%), ¹⁸⁵ W (3%)	

- Detritiation of the breeder considered: 99 %
- After 1 year of radioactive decay, few nuclides leading to more than 2W/t
- After 50 years, no HLW issue linked to decay heat anymore



Detritiation of the breeder required to limit radioactive decay needs

Waste classification status – ILW assessment



WCLL Components		Dominant nuclides			
		Above UK LLW $\beta+\gamma$ limit		Above French LLW limit	
		at 20 years	at 50 years	at 20 years	at 50 years
Blanket (detritiation 99%)	Inboard	³ H (65%), ⁵⁵ Fe (34%), ⁶⁰ Co (1%)	³ H (99%)	³ H, ⁹⁴ Nb	³ H, ⁹⁴ Nb
	Outboard	³ H (63%), ⁵⁵ Fe (36%), ⁶⁰ Co (1%)			
Limiter		⁵⁵ Fe (69%), ⁶⁰ Co (17%), ⁶³ Ni (13%)	⁶⁰ Co (3%), ⁶³ Ni (94%)	⁹⁴ Nb	⁹⁴ Nb
Divertor		⁵⁵ Fe (81%), ⁶⁰ Co (14%), ⁶³ Ni (5%)	³ H (1%), ¹⁴ C (2%), ⁵⁵ Fe (1%), ⁶⁰ Co (6%), ⁶³ Ni (89%)	⁹⁴ Nb	⁹⁴ Nb

In-vessel components, above the LLW after 50yrs:

- In UK
 - ³H for the blankets, ⁶³Ni for the limiters and the divertor
- In France
 - ⁹⁴Nb

WCLL Components	Dominant nuclides			
	Above UK LLW $\beta+\gamma$ limit		Above French LLW limit	
	at 20 years	at 50 years	at 20 years	at 50 years
Upper and equatorial port	⁶⁰ Co (19%), ⁶³ Ni (71%)	⁶³ Ni (98%)		
Lower Port	⁵⁵ Fe (13%), ⁶⁰ Co (18%), ⁶³ Ni (67%)	⁶³ Ni (97%)		
Vacuum vessel (inboard)	⁵⁵ Fe (49%), ⁶⁰ Co (22%), ⁶³ Ni (27%)	⁶³ Ni (93%)		
Vacuum vessel (shell)	⁵⁵ Fe (15%), ⁶⁰ Co (27%), ⁶³ Ni (55%)	⁶³ Ni (95%)		
Vacuum vessel (outboard)	⁵⁵ Fe (54%), ⁶⁰ Co (21%), ⁶³ Ni (23%)	⁶³ Ni (93%)		

Ports and VV

- Above the LLW threshold in UK after 50 yrs because of ⁶³Ni
- Below the LLW threshold in France

Bioshield, cryostat, intercoils shield and coils:

- Below the LLW threshold both in UK and France few hours after shutdown

HCPB vs WCLL, main differences:

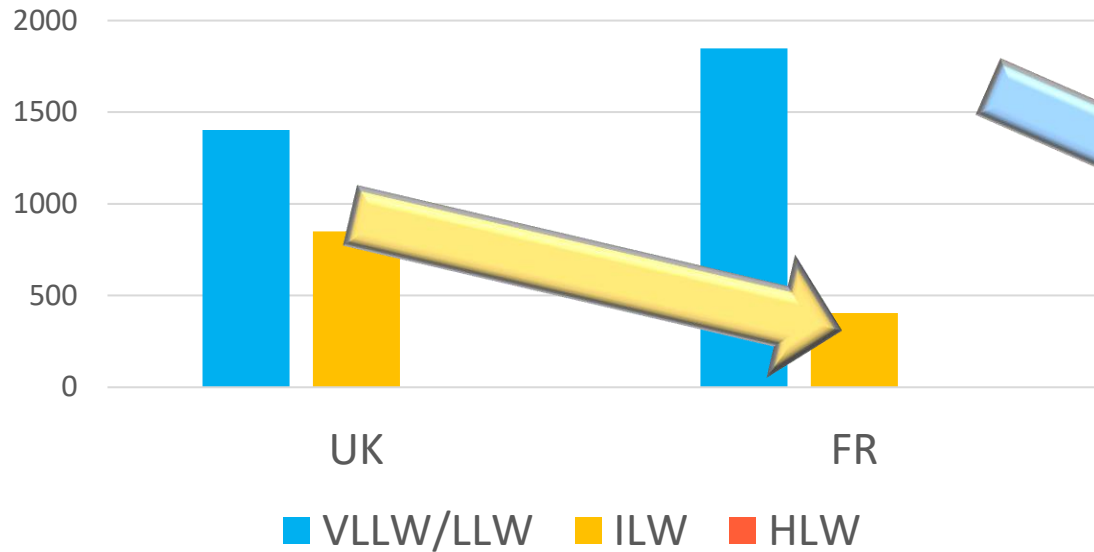
- VV inboard and shell: LLW → ILW after 50 yrs in France because of ^{94}Nb
- The ILW blanket classification also due to limits on α emitters
 - ^{239}Pu (for 32%) and ^{241}Am (for 49%) because of U impurity in Be_{12}Ti .

50 dpa vs 20 dpa, main differences:

- Some additional nuclides become responsible for the BB ILW classification:
 - UK: ^{14}C from KALOS, Be_{12}Ti and EUROFER
 - France: $^{108\text{m}}\text{Ag}$ from W and Be_{12}Ti

Waste classification status

WCLL mass repartition at 50 years (tons)

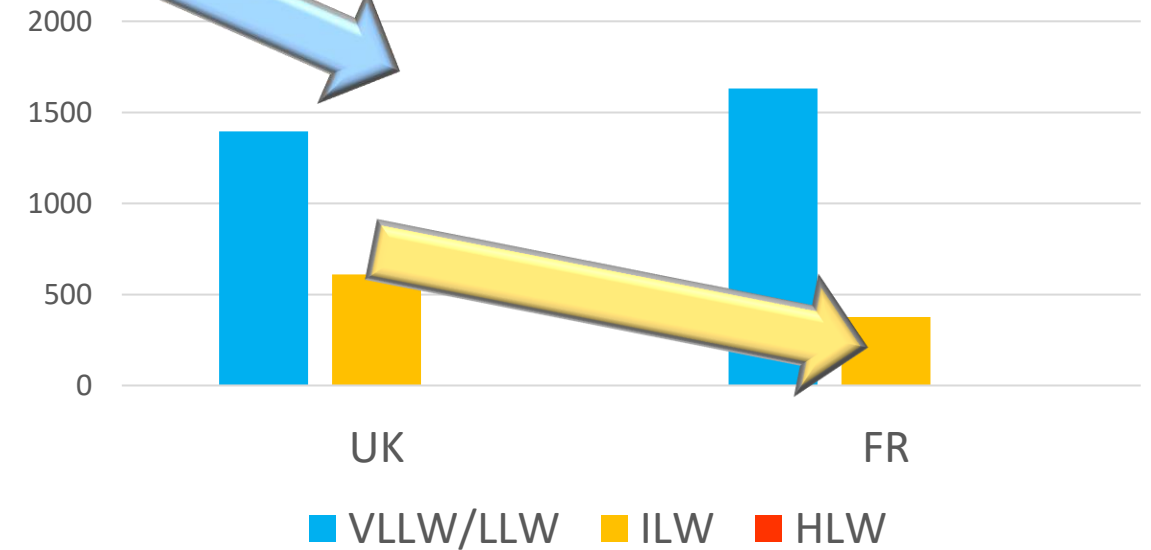


Less ILW with French classification

No HLW due to decay heat

Less waste with HCPB

HCPB mass repartition at 50 years (tons)

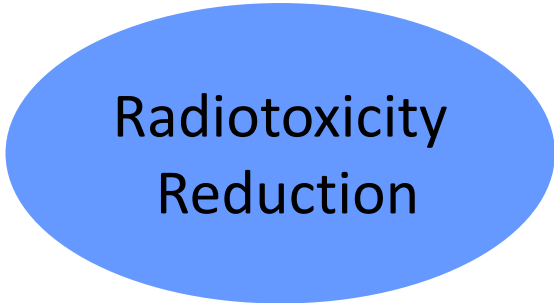




Nuclides of interest

- Tritium → detritiation
 - ^{14}C (from ^{14}N) → decarburization
 - ^{63}Ni (from ^{62}Ni)
 - ^{94}Nb (from ^{93}Nb)
- } → Optimization of Ni and Nb contents

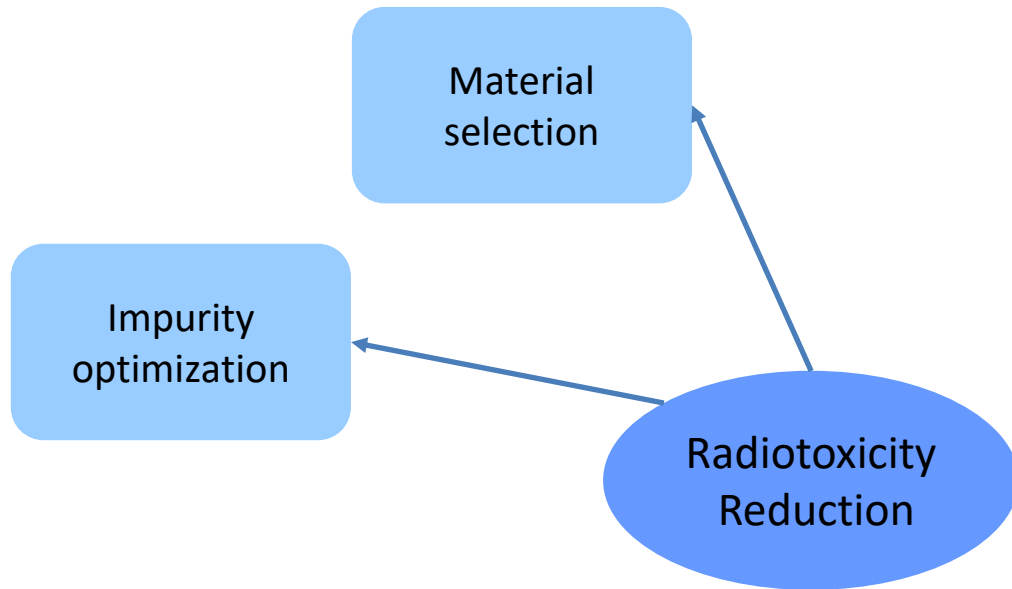
Challenges

A blue oval containing the text 'Radiotoxicity Reduction'.

Radiotoxicity
Reduction

A green oval containing the text 'Waste amount Reduction'.

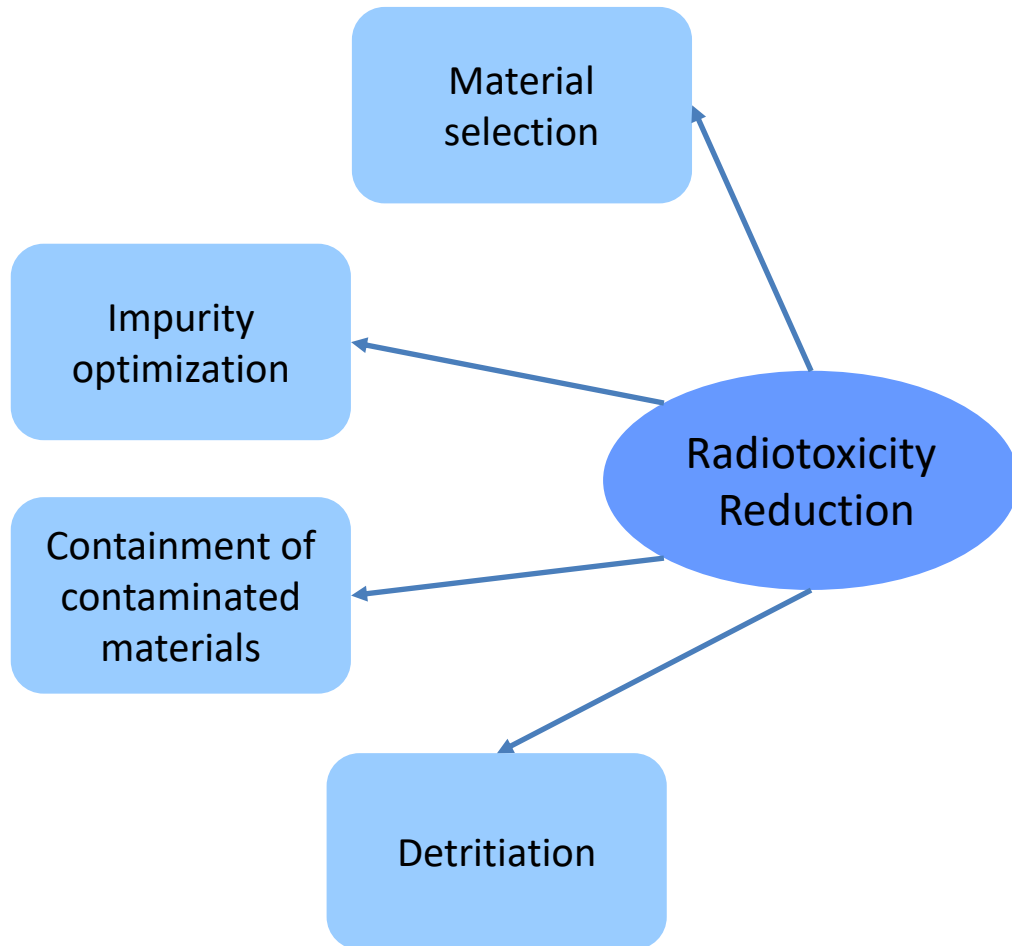
Waste
amount
Reduction



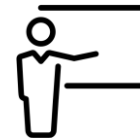
- Reduced Activation Ferritic-Martensitic steel EUROFER97
 - Reduced concentration on detrimental impurities: Mo, Ni, Al, Nb, Co and Cu vs SS316LN
 - Further reduction with EUROFER batch 3:
 - 90% for Nb, 5% for N and 15% for Ni

→ BB moving faster from ILW to LLW in France

HCPB blanket		Time to LLW (yrs)
Inboard	EUROFER	> 100 (⁹⁴ Nb)
	EUROFER B3	1
Outboard	EUROFER	> 100 (⁹⁴ Nb)
	EUROFER B3	5



- Anti-permeation and corrosion barrier coatings for WCLL
 - Less T permeation and less Activated Corrosion products
 - Al based coatings
- Detritiation
 - Thermal desorption under atmospheric air w/wo gaseous hydrogen, melting under vacuum, static hydrogen atmosphere or argon flow

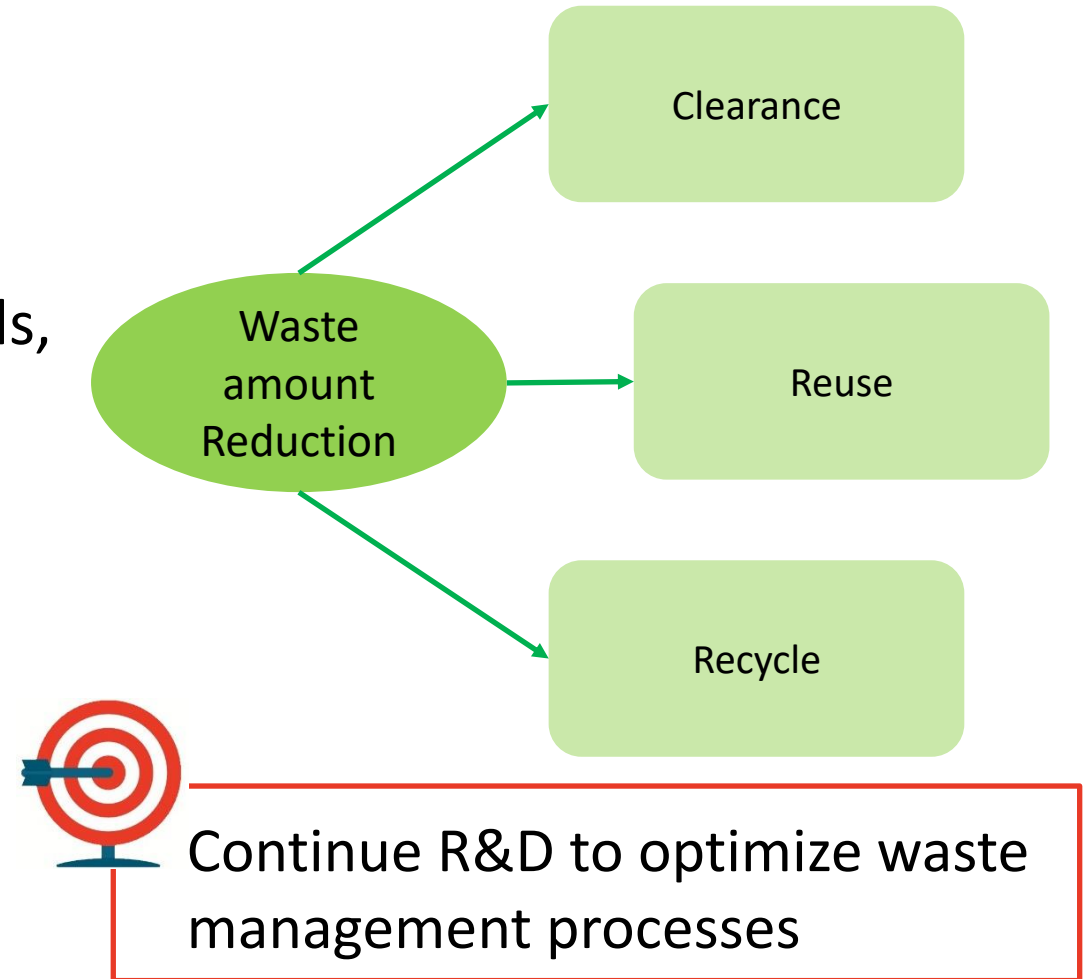


This Thursday

P5D1: Mark Gilbert

Fusion waste requirements for tritium control: perspectives and current research

- Clearance to reduce the amount of radioactive materials that will have to be considered as nuclear waste
- Recycling & reuse will also become essential
 - Segregation of mixed activated materials,
 - Processes to remove detrimental isotopes (removal of “slag” from melts)
 - Management of secondary waste,
 - Expected properties of recycled materials,
 - Manufacturing of component using radioactive materials as raw materials,
 - Radioactive build up in materials...

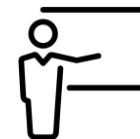


Perspectives for EU DEMO

EUROfusion R&D programmes to fulfil the high level plant requirements on waste and decommissioning.

- Establishment of inventories for solid, liquid and gaseous waste stream
- Treatments to be developed inside and outside the plant to facilitate their management in final disposal
 - Materials Detritiation Facility (MDF) at UKAEA
 - Tritium levels after processing **below 100 Bq/g**.
 - Work is on-going by assessing impact of **temperature** (between 600 and 1000°C), **flow rates** (between 250 and 1000 l/min), **ramp rate** (between 2.5 and 10°C/min) and **holding time** (between 0 and 24h)
 - **Reproducibility** impacted by current limitations of the process (flow and tritium monitoring, memory effect between detritiation batches...) → optimization

- Dust detritiation → **sintering** at ENEA/RINA
 - Distributed pores, open porosity and large metal surface for efficient detritiation (**removal of 50 to 70 %** of the absorbed hydrogen simulating tritium)
 - Transform dust into a **massive product** facilitating handling and final disposal by avoiding any radioactive dust dispersion
- **Next plans**
 - Test technologies for activated steel treatment including optimization the waste recycling process
 - Reduce the constraints on the management of waste such as mercury contained within the pumping systems, PbLi (including secondary waste from PbLi decontamination), pebbles or getter beds...
 - Outline a first decommissioning plan



This Thursday

P5D2: Oliver Gastaldi

Overview of French R&D studies for the development of tritium confining packages



As a conclusion

- Waste evaluation
 - Evaluations of the waste classification are regularly performed to assess impact of design choices
 - Last evaluation has shown that no waste will require HLW disposal if efficient detritiation is performed
 - ILW can't be avoided with current design and analysed disposal and effort should continue to reduce amounts of Nb and Ni in EUROFER
- EUROfusion R&D programme developed to limit waste burden on the next generations
- The ultimate goal at conceptual phase → identify any showstopper and identify the needs for the Active Maintenance Facility and Waste Treatment Facility.

Thanks for your attention



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