

# Compatibility assessments for fusion applications: Sn, Li, Pb-Li and FLiBe

Bruce Pint, Marie Romedenne and Dino Sulejmanovic

Corrosion Science and Technology Group  
Materials Science and Technology Division  
Oak Ridge National Laboratory

ISFNT, September 2023

ORNL is managed by UT-Battelle, LLC for the US Department of Energy

# Acknowledgments

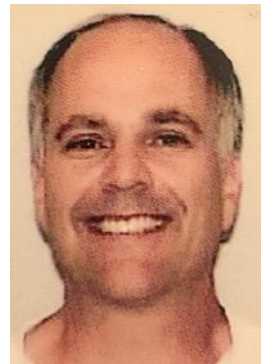
- Funding
  - U.S. Dept. of Energy, Office of Fusion Energy Sciences (**Kessel**, Humrickhouse, Smolentsev)
  - U.S.-Japan FRONTIER project (Sn/ODS FeCrAl, Prof. M. Kondo, task co-leader)
  - ORNL Laboratory Directed Research & Development SEED funding (FLiBe)
- ORNL team
  - Adam Willoughby, Mike Stephens, Brandon Johnston, Jiheon Jun: LM experimental work
  - Shane Hawkins, Kelsey Hedrick: tensile testing
  - Characterization: Tracie Lowe, Victoria Cox, Ercan Cakmak, Yi-Feng Su (TEM)
- T. Nozawa, QST, Japan: F82H plate
- Mentors: Jack DeVan, Jim DiStefano, Peter Tortorelli, Steve Pawel



DeVan 1929-2000



DiStefano 1935-2013



2013 APMT TCL design

# ORNL compatibility research has several current tasks

- **US DOE FESS LM PFC project (2020-2025)**
  - Investigating liquid metal **embrittlement of F82H (Fe-8Cr-2W) in Li**
- **US-Japan FRONTIER emphasis on Sn (2019-2024)**
  - Pre-oxidized FeCrAl (ODS, APMT): Sn thermal convection loop (2021)
  - HFIR irradiation pre-oxidized FeCrAl in Sn at 400°C (**0.8 dpa in 2022**)
- **US DOE Blanket & Fuel cycle project (2019-2024)**
  - ORNL Pb-Li project ended 2019 (4 monometallic APMT (FeCrAlMo) loops)
  - More fusion relevant materials in **flowing Pb-Li** (APMT tubing)
    - **TCL #5: SiC, ODS FeCrAl (700°C peak, completed April 2020)**
    - **TCL #6: SiC, Al-coated RAFM (650°C peak, completed in September 2021)**
    - **TCL #7 : SiC, Al-coated RAFM (650°C peak, 2000 h operation completed Sept. 2023)**
- **ORNL SEED: explore steel-Be<sub>12</sub>Ti interaction in FLiBe (2023)**
  - Initial static capsule testing in FLiBe at 550°-750°C in September 2023

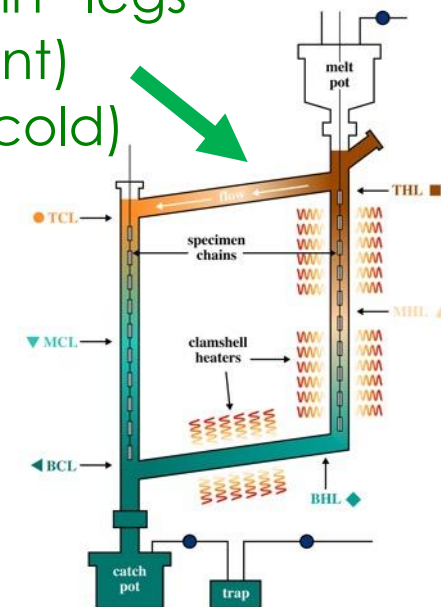
# Liquid physical properties and compatibility TRL

| Property                        | Li                               | Pb-Li                         | Sn         | FLiBe        |
|---------------------------------|----------------------------------|-------------------------------|------------|--------------|
| Melting Temp. (°C)              | <b>181</b>                       | 235                           | 232        | <b>459</b>   |
| Density (g/cm <sup>3</sup> )    | <b>0.5</b>                       | <b>9.9</b>                    | 6.5        | 2.0          |
| Viscosity (N•s/m <sup>2</sup> ) | 0.0006                           | <b>1.4</b>                    | 0.002      | 0.07         |
| Heat capacity (J/kg•K)          | <b>4170</b>                      | 190                           | 248        | 2414         |
| Thermal Conductivity (W/m•K)    | <b>65</b>                        | 25                            | 33         | <b>1.1</b>   |
| Electrical Conductivity (μΩ•cm) | 25                               | 1                             | 48         | 0.4          |
| Compatibility TRL               | <b>high</b>                      | <b>highest</b>                | <b>low</b> | <b>lower</b> |
| Thoughts                        | MHD mitigation,<br>No SiC, No Ni | Radiation?<br>Magnetic field? | Corrosive  | ??           |

**All concepts are far from where they need to be for designing DEMO/FPP**

# How do we assess and quantify LM compatibility?

- Thermodynamics
  - First screening tool (assessments published, but data is not always available)
- Static capsule/crucible (**screening test only**)
  - Isothermal test, first experimental step
  - Prefer inert material and welded capsule to prevent impurity ingress
  - **Dissolution rate changes with time**: key ratio of liquid/metal surface
  - **No assessment of mass transfer**
- Flowing thermal convection loop (TCL)
  - Flowing liquid metal by heating one side of “harp” with specimen chain in “legs”
  - Relatively slow flow and  $\sim 100^{\circ}\text{C}$  temperature variation (design dependent)
  - **Captures solubility change in liquid**: dissolution (hot) and precipitation (cold)
    - Dissimilar material interactions between specimens and loop material
- Flowing forced convection or pumped loop
  - Most realistic conditions for flow
  - Historically, similar qualitative corrosion results as TCL at 10+X cost
  - Necessary progression for other aspects of LM blanket development
  - **Need results ASAP, including with magnets and radiation**



# Liquid metal plasma facing components? Li vs. Sn

Li has high vapor pressure

But better Li-RAFM compatibility

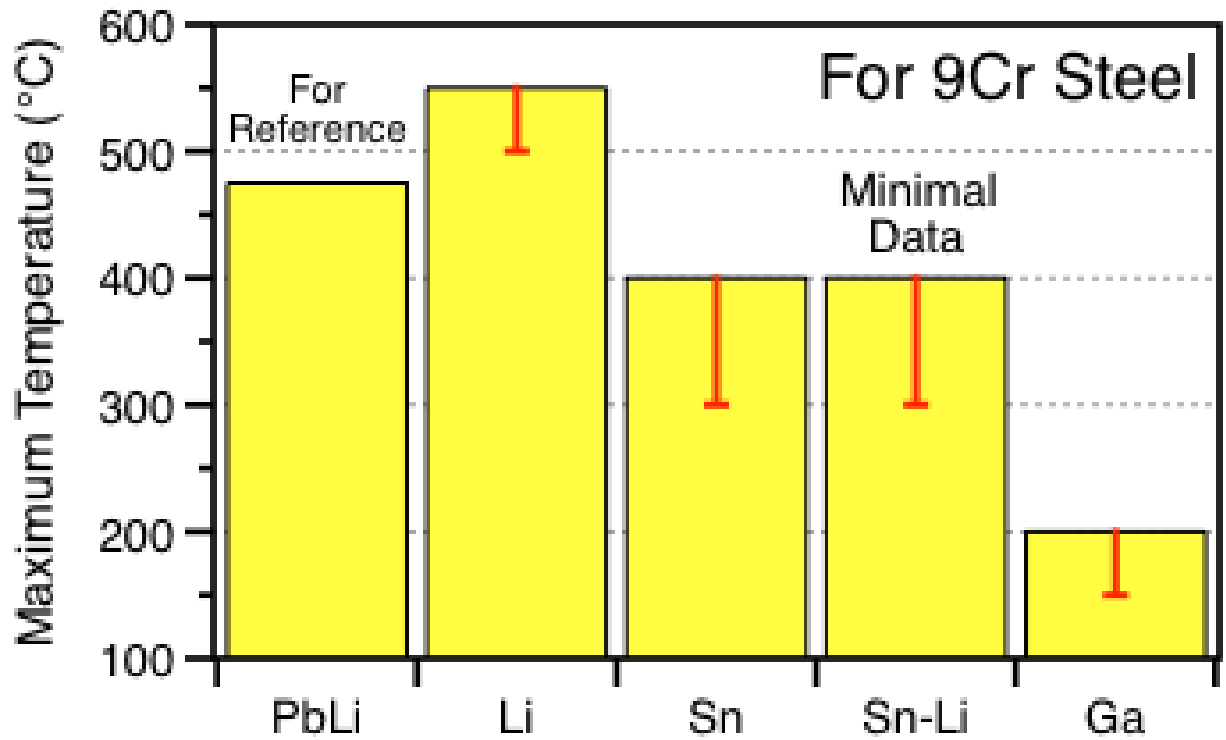
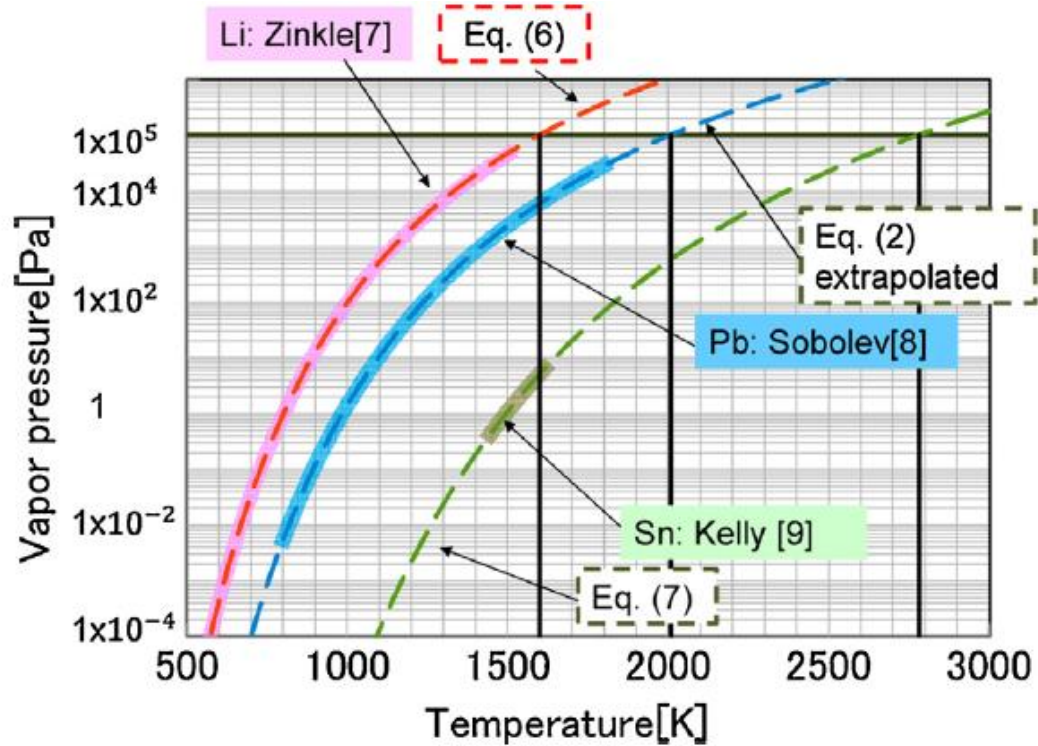


Fig. 1. Vapor pressure of Li, Pb, and Sn given in [7-9] and from Eqs. (2), (6) and (7) for extrapolation.

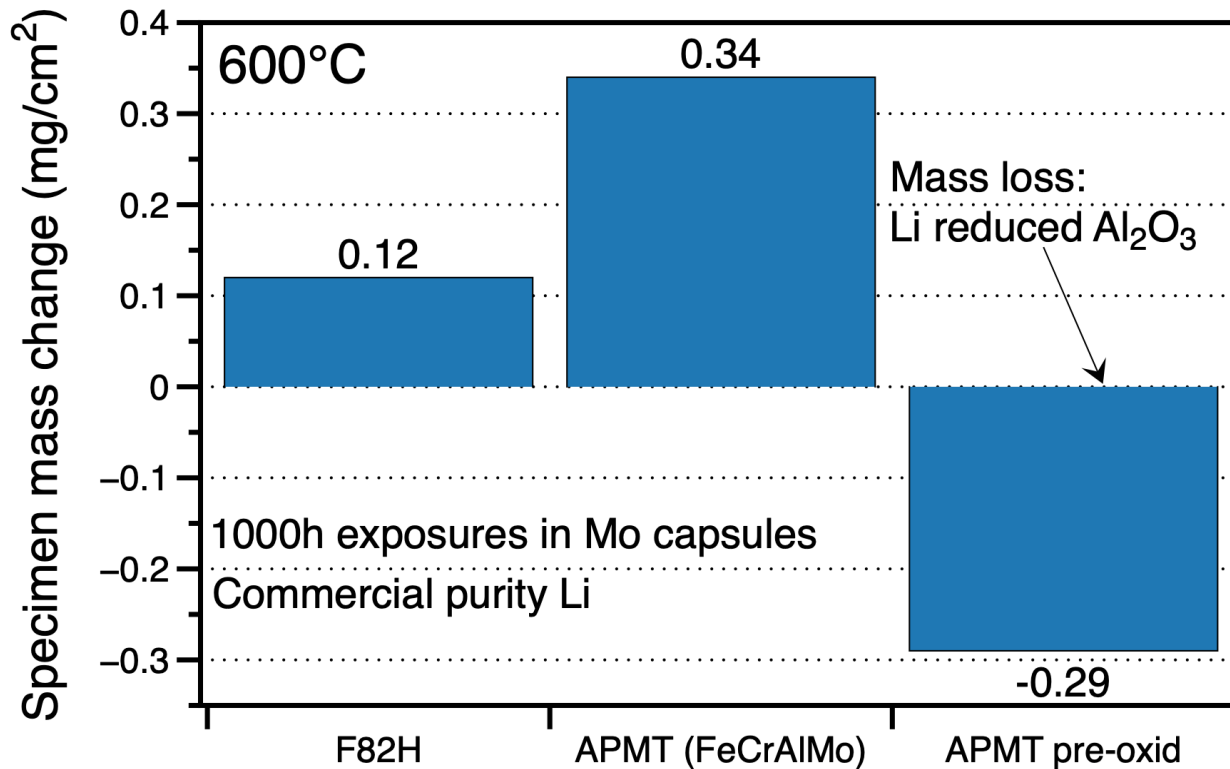
From Kondo et al.

#1 Is Li liquid metal embrittlement a concern?

#2 can Sn be compatible?

# Li capsule testing: minimal mass changes at 600°C/1000 h

## Mass change after 1000h in Mo capsule



F82H: Fe-8Cr-2W

APMT: Fe-20Cr-5Al-3Mo+Y,Zr,Hf,Ti,O

Preox = pre-oxidation for 2h at 1000°C

## F82H: OK with Li at 600°C

## Static capsule testing:

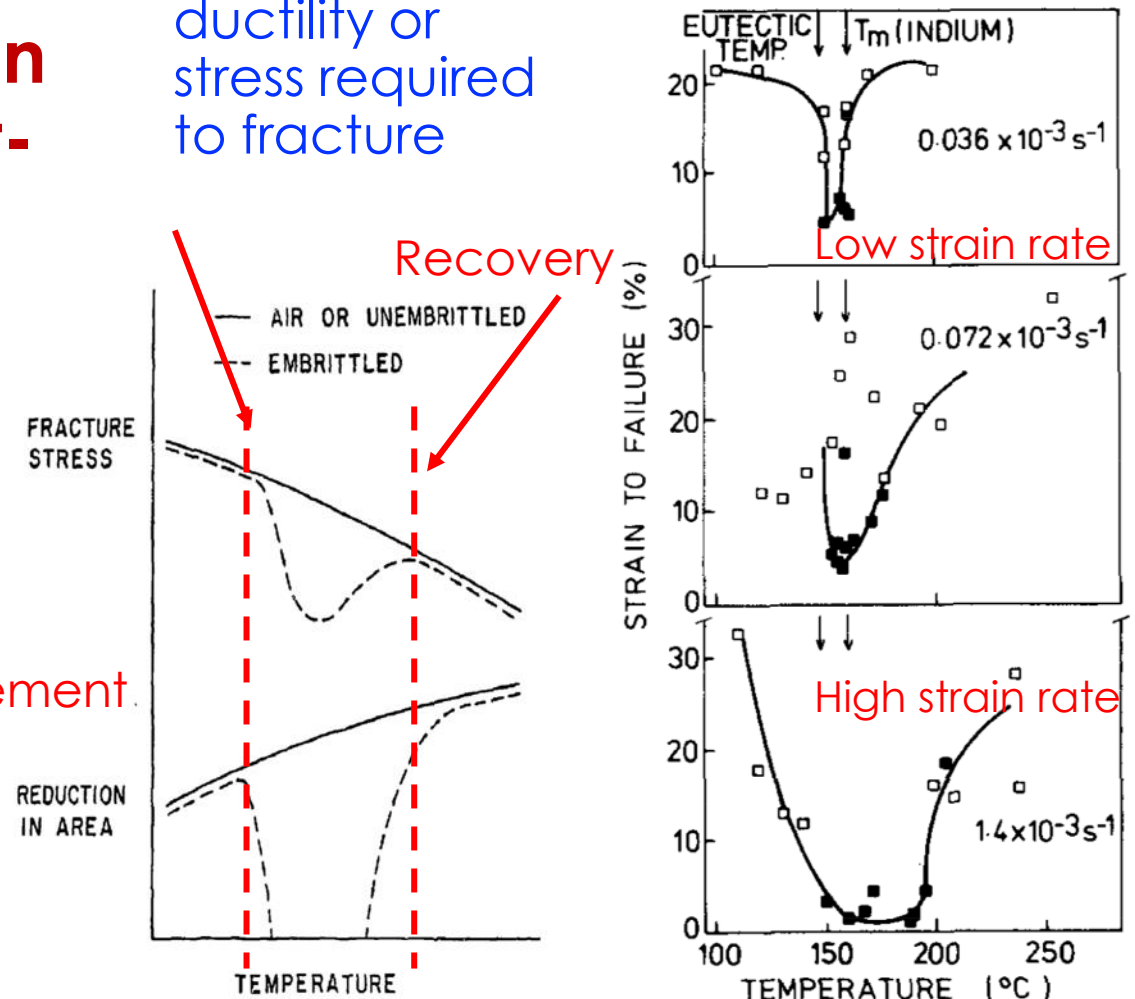
Thermodynamics:  
 $6\text{Li} + \text{Al}_2\text{O}_3 \rightarrow 3\text{Li}_2\text{O} + 2\text{Al}$



# Li Liquid Metal Embrittlement (LME) is still a concern

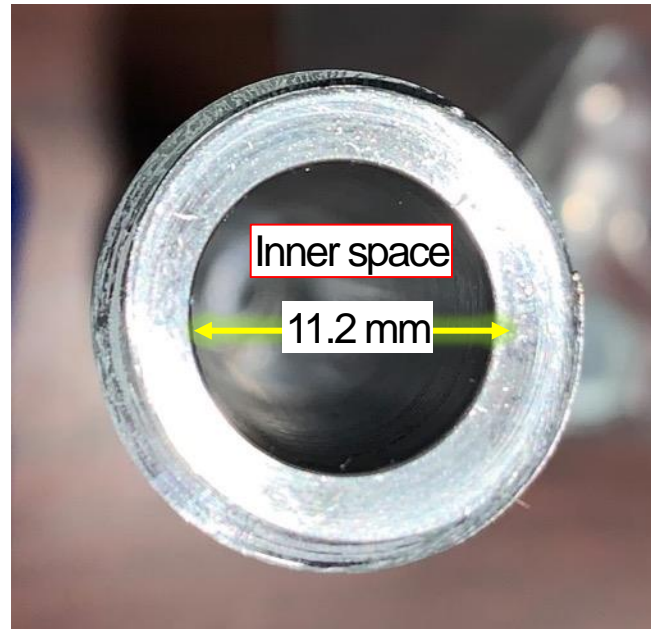
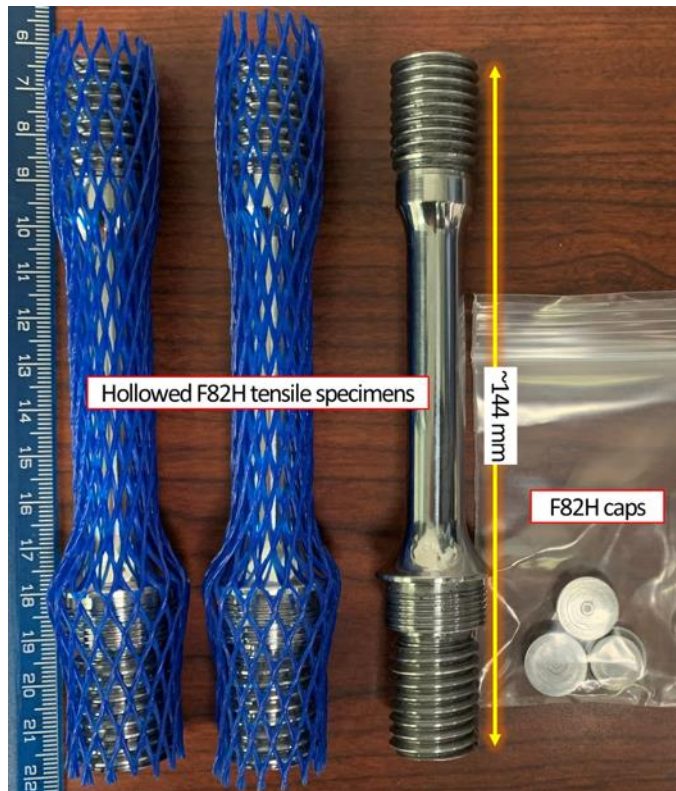
- Temperature near Li  $T_m = 181^\circ\text{C}$
- **Traditional differentiation between long-term degradation and short-term LME fracture**
- Role of wetting?
  - Wetting needed for corrosion
- BUT wetting not needed if:
  - Native oxide fractures
- **Is F82H susceptible to Li LME?**

Reduction in ductility or stress required to fracture



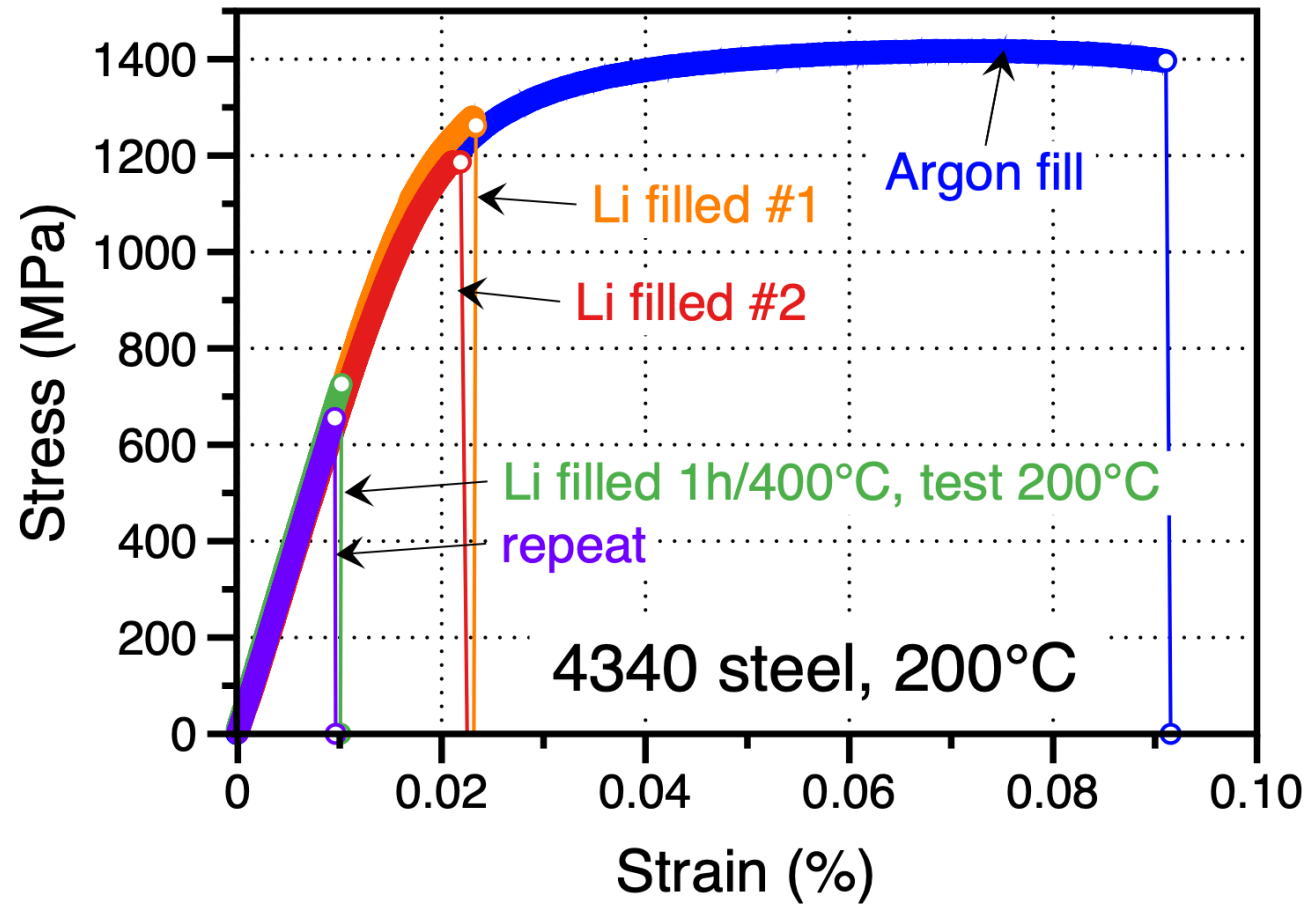


# Hollow specimens were machined for safe LME testing



- F82H: Fe-8Cr-2W plate from Japan QST
- 4340 steel (1.8%Ni,0.8%Cr,0.25%Mo,0.4%C)
- 200°C tensile test per ASTM E21
  - Near Li melting point (181°C)
  - Strain rate 0.005/min
  - Controlled Ar environment (no extensometer)

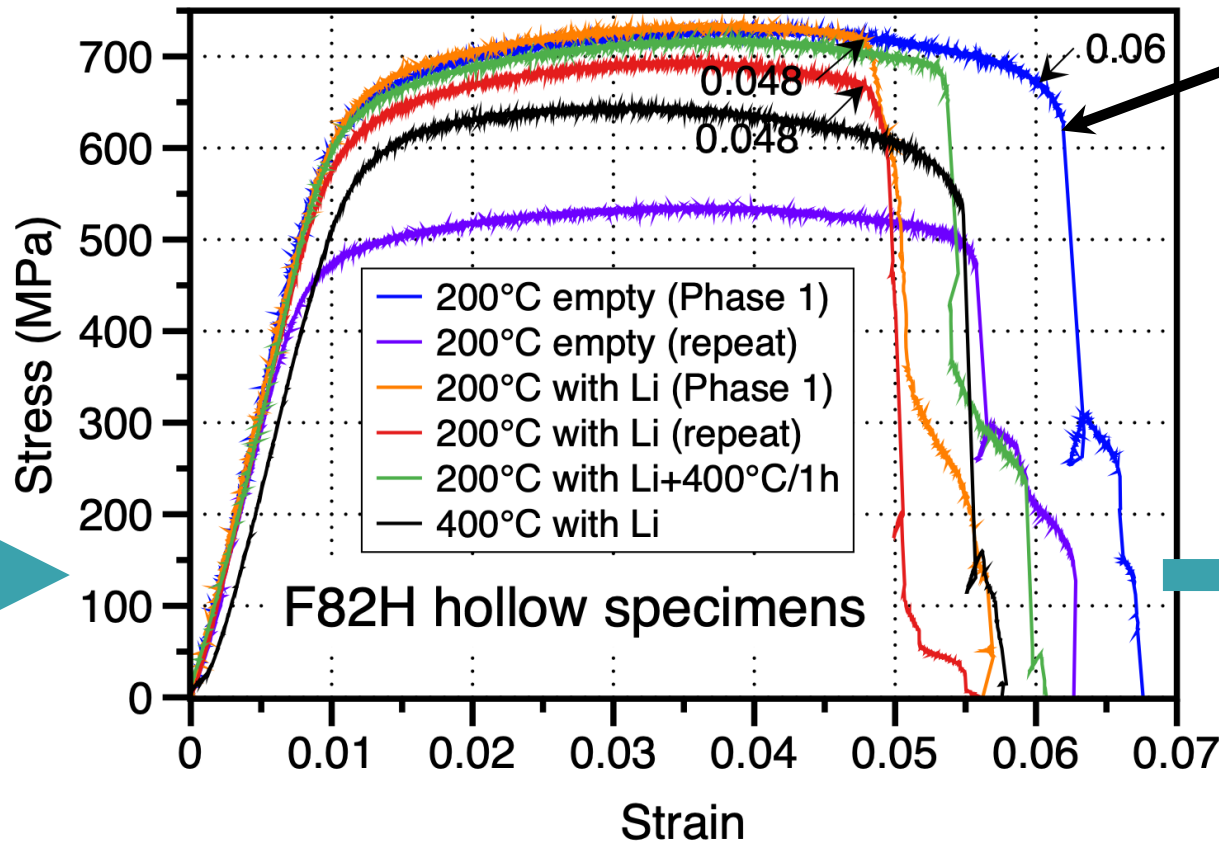
# 4340 steel: demonstrated hollow specimen methodology



- All 200°C tensile tests, 0.005/mm strain rate
- Plus 400°C/1h anneal for wetting
- Reproducible results

# Hollow F82H tensile specimens: no indication of Li embrittlement

Tensile test at 200°C or 400°C: 0.005/min strain rate per ASTM E21



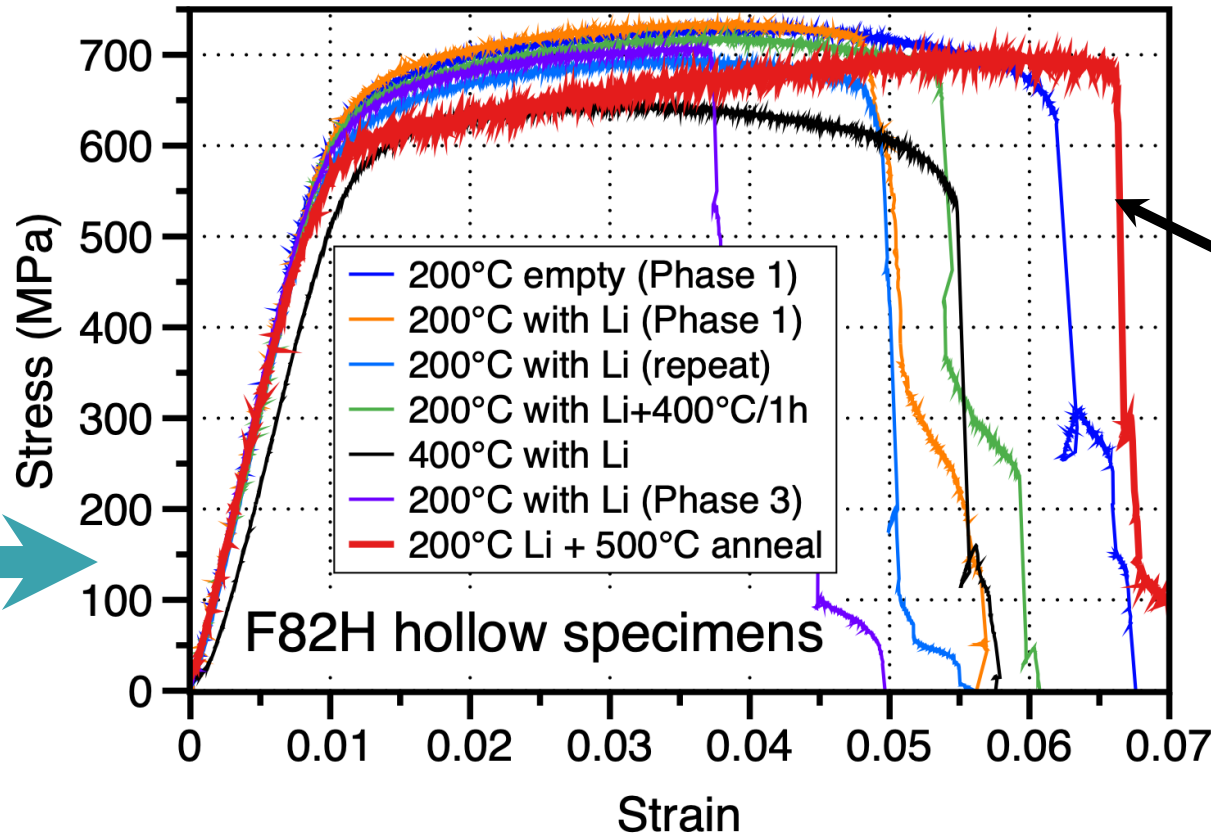
One empty specimen (no Li)



Li-filled F82H: Fe-8Cr-2W  
tensile specimens

# Hollow F82H tensile specimens: no indication of Li embrittlement

Tensile test at 200°C or 400°C: 0.005/min strain rate per ASTM E21



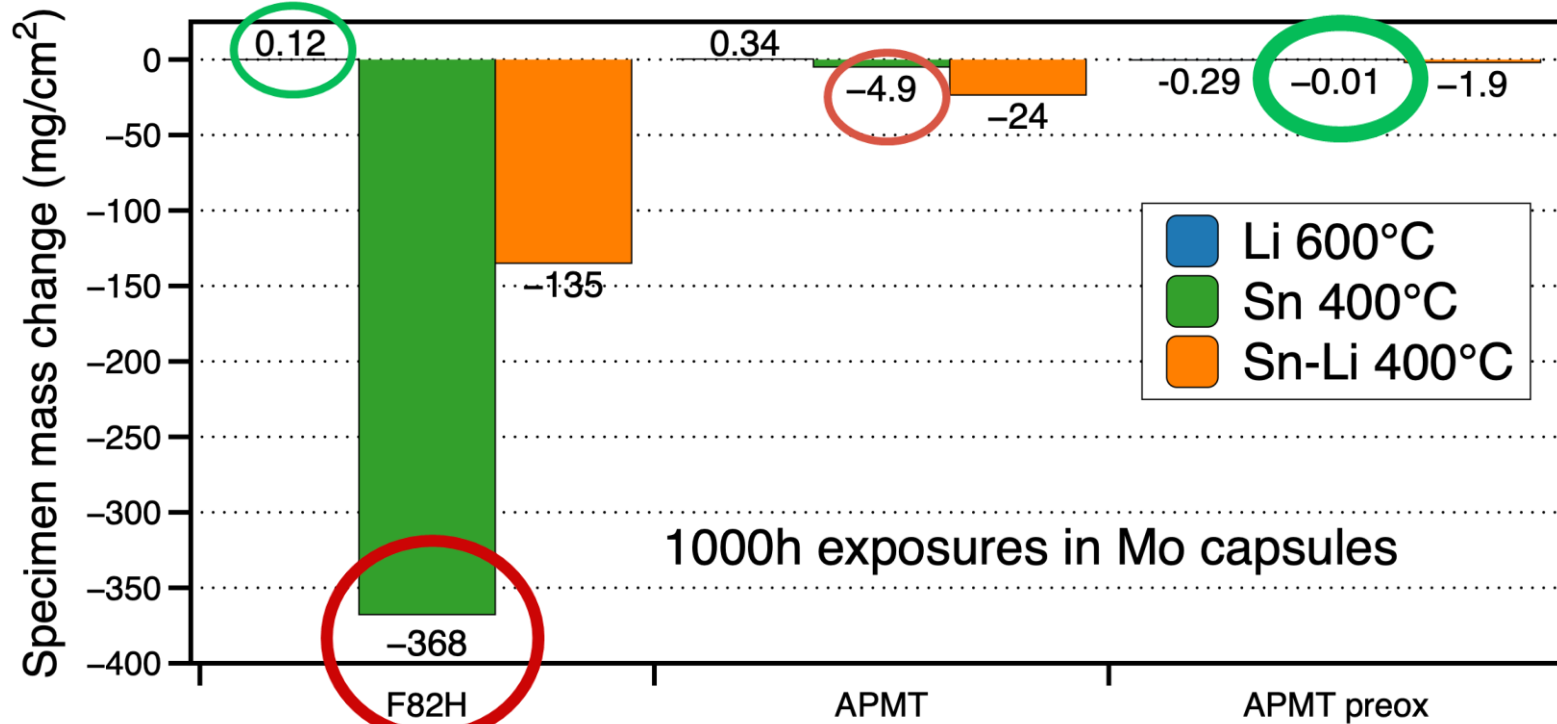
Specimen annealed  
500°C/500h

Li-filled F82H: Fe-8Cr-2W  
tensile specimens

Manuscript nearly complete:  
Romedenne et al. for submission

# Sn: bad for F82H at 400°C, good for pre-oxidized FeCrAl

Mass change after 1000h in Mo capsule + Li cleaning



F82H: Fe-8Cr-2W

APMT: Fe-20Cr-5Al-3Mo+Y,Zr,Hf,Ti,O

Preox = 2h/1000°C

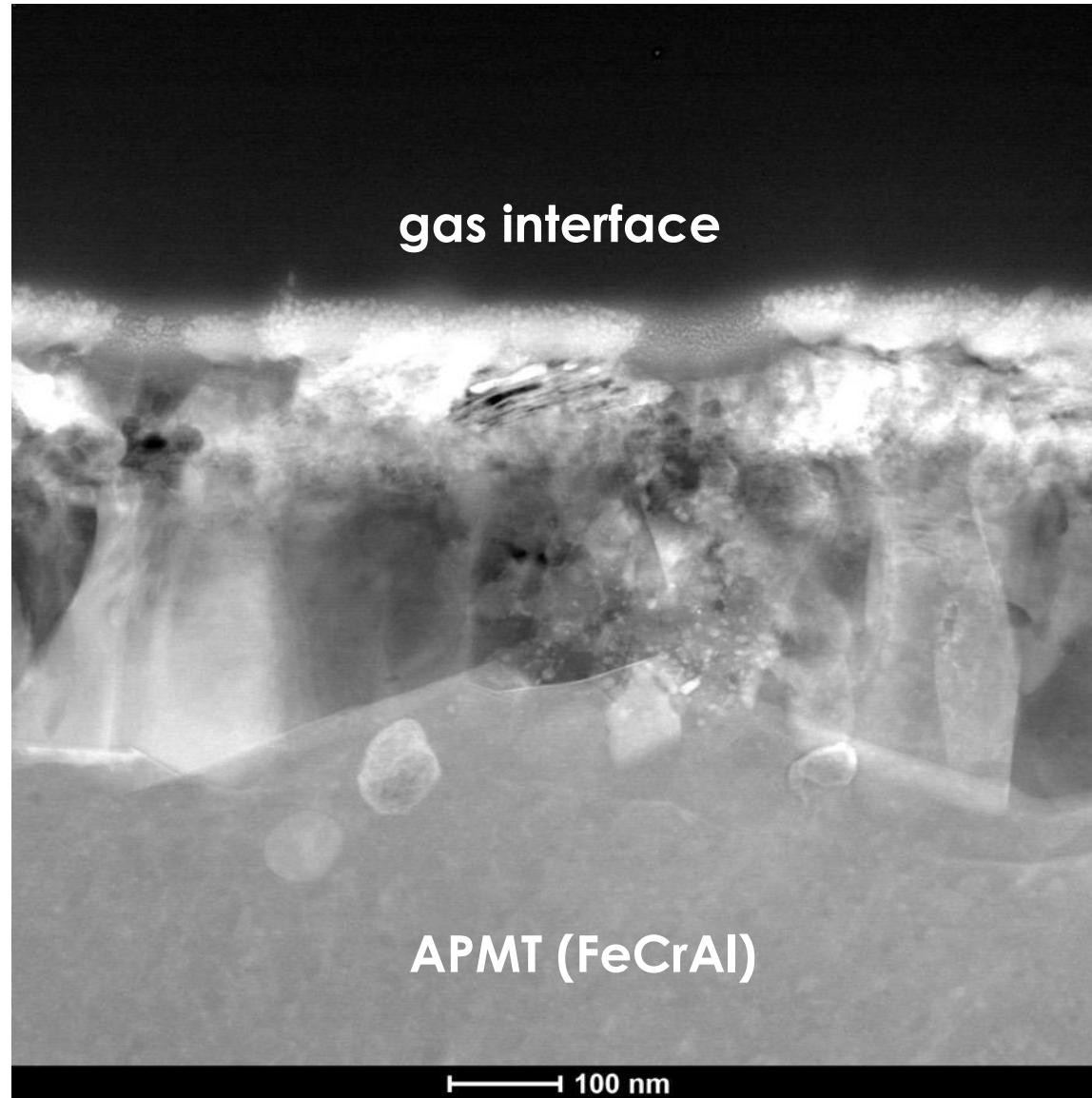
- #1 F82H: not compatible with Sn
- #2 Sn-Li mass loss for all: no further work
- #3 Need flowing test for pre-ox FeCrAl in Sn

Static capsule testing:



# Thin $\alpha$ -Al<sub>2</sub>O<sub>3</sub> layer formed on APMT after 2 h at 1000°C in air

~400 nm thick



Equiaxed grains  
Mixed Fe, Cr, Al oxides

Columnar  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> grains

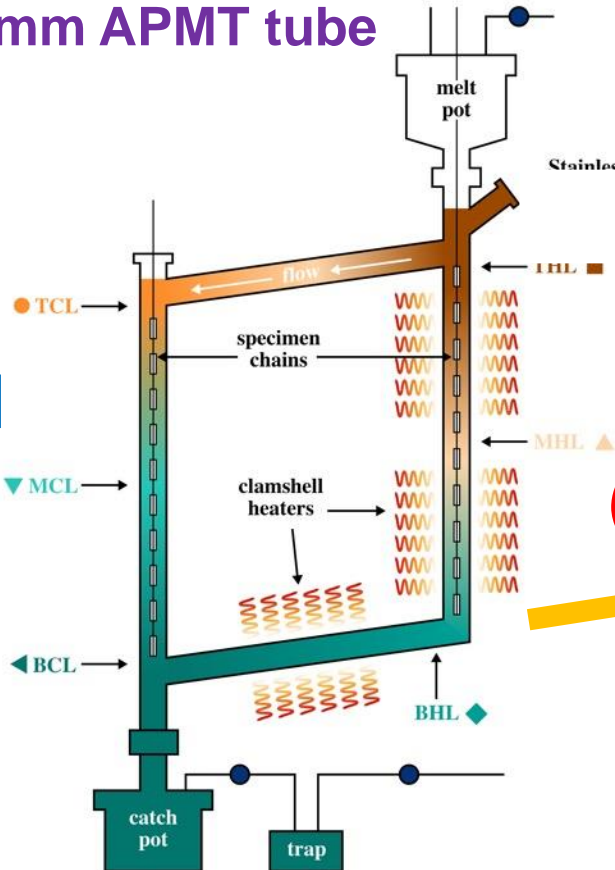
# TCL: 2 specimen chains in the hot and cold legs of loop

0.75m tall

0.5m wide

26.7mm APMT tube

Cold  
Leg  
(CL)



Hot  
Leg  
(HL)



Three materials exposed:

APMT: Fe-20Cr-5Al-3Mo+Y,Zr,Hf,Ti,O

ORNL ODS: Fe-10Cr-6Al-0.2Y-0.3Zr

Japan ODS: Fe-12Cr-6Al-0.4Y-0.4Zr-0.5Ti

All pre-oxidized 2h/1000°C to form  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> surface layer (0.5µm thick)

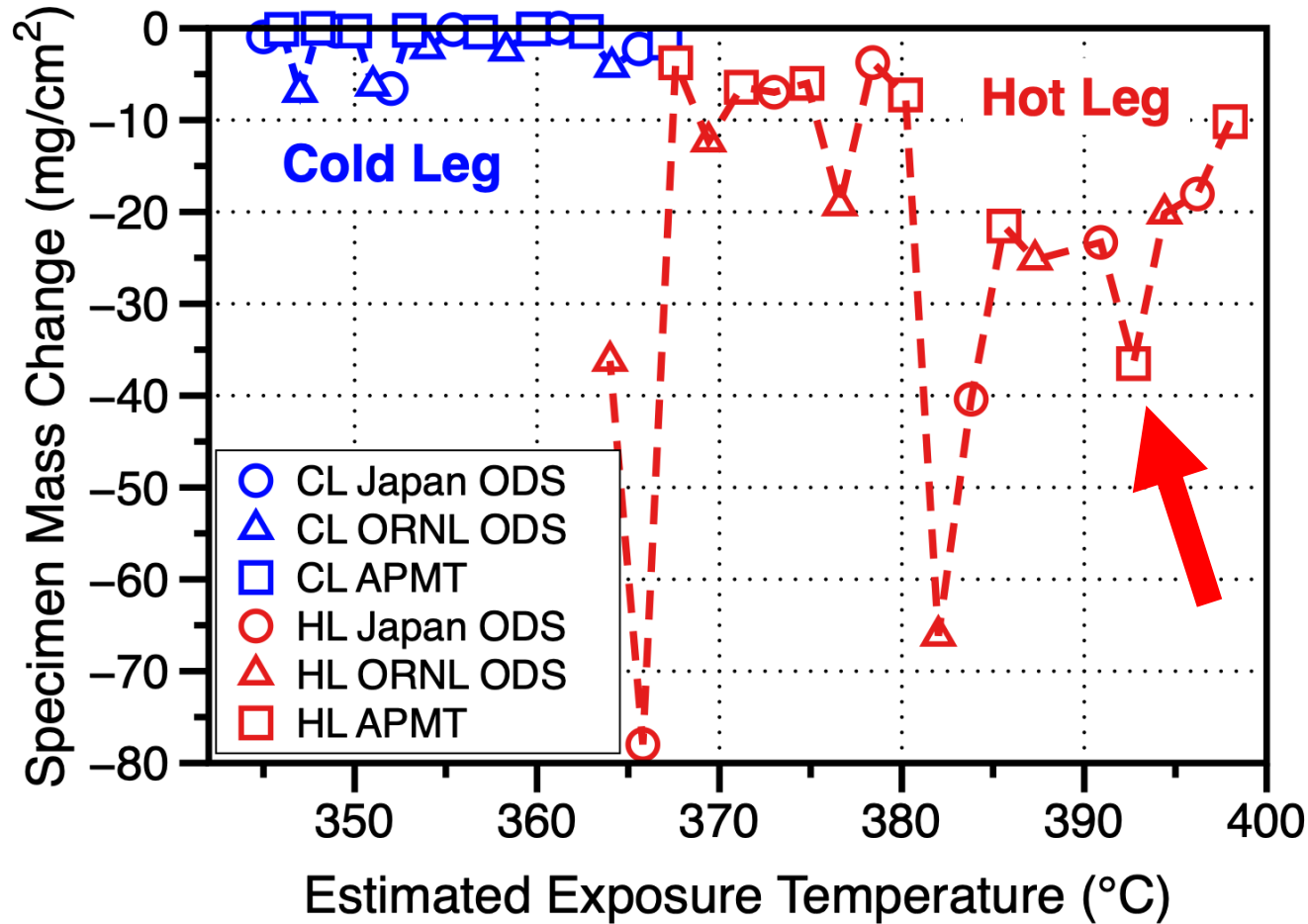
Peak temperature: 400°C

Temperature gradient: 55°C

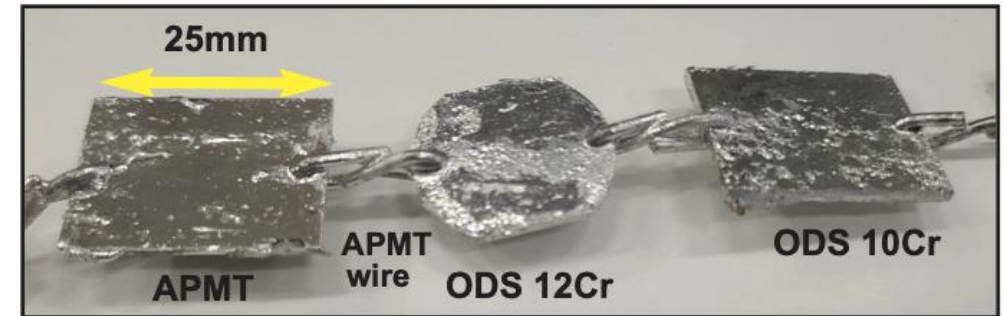
Velocity: ~1 cm/s



# Mass change data from Sn loop (1000 h/350°-400°C)



Specimens had Sn remaining on surface after removal  
 - Removed by dipping in Li at 250°C



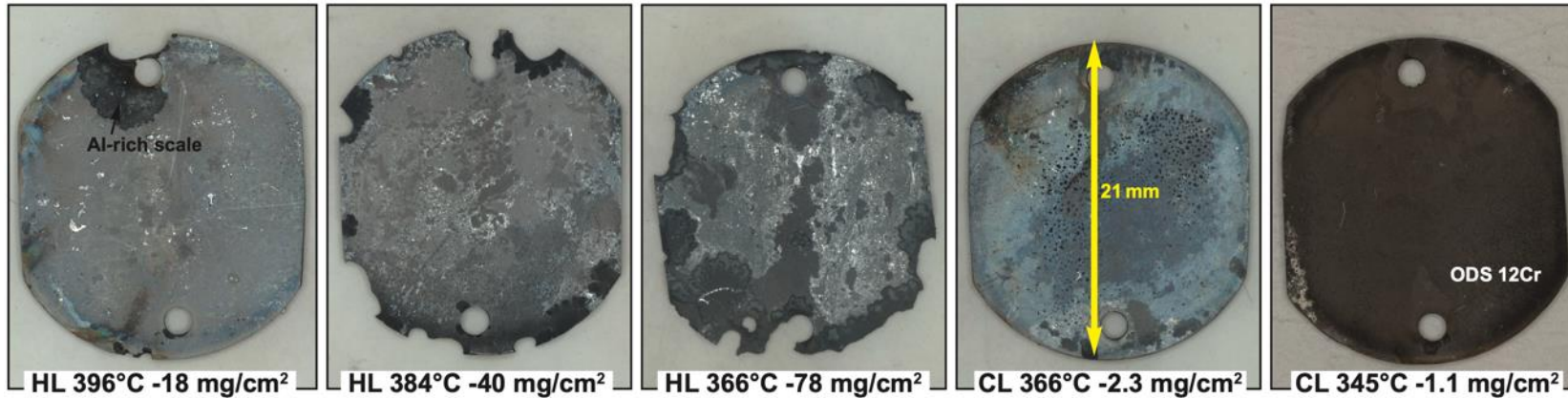
Coupons: 19 x 25 x 1 mm

APMT: Fe-20Cr-5Al-3Mo+Y,Zr,Hf,Ti,O  
 Japan ODS: Fe-12Cr-6Al+Zr,Y  
 ORNL ODS: Fe-10Cr-6Al+Zr,Y

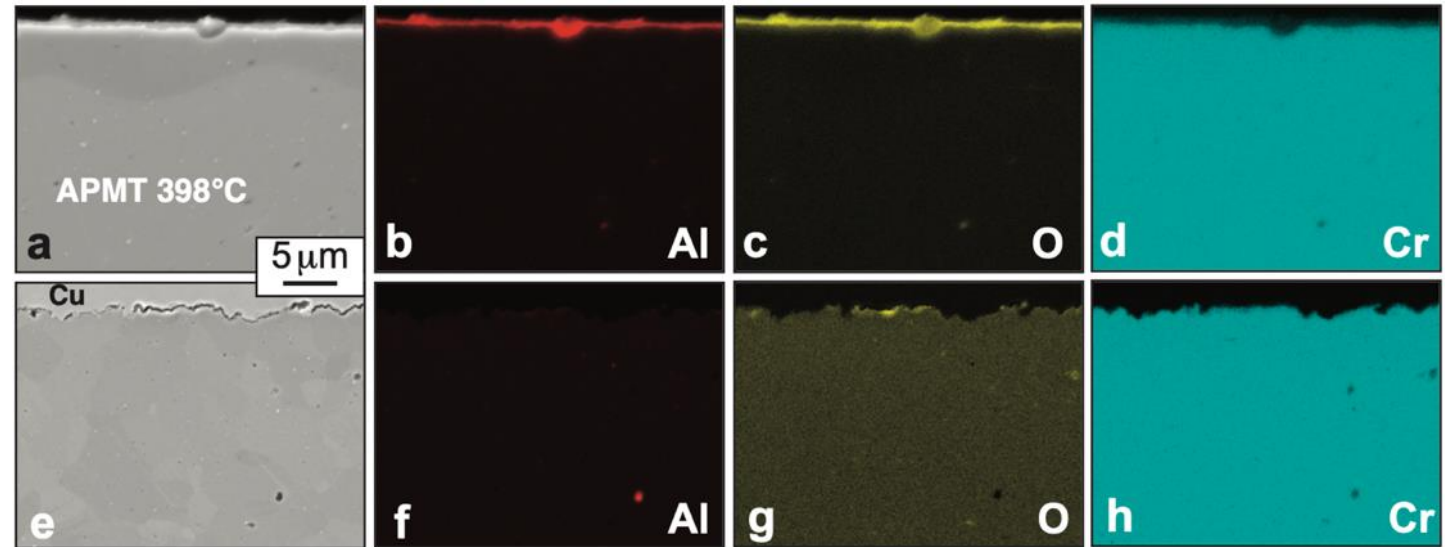
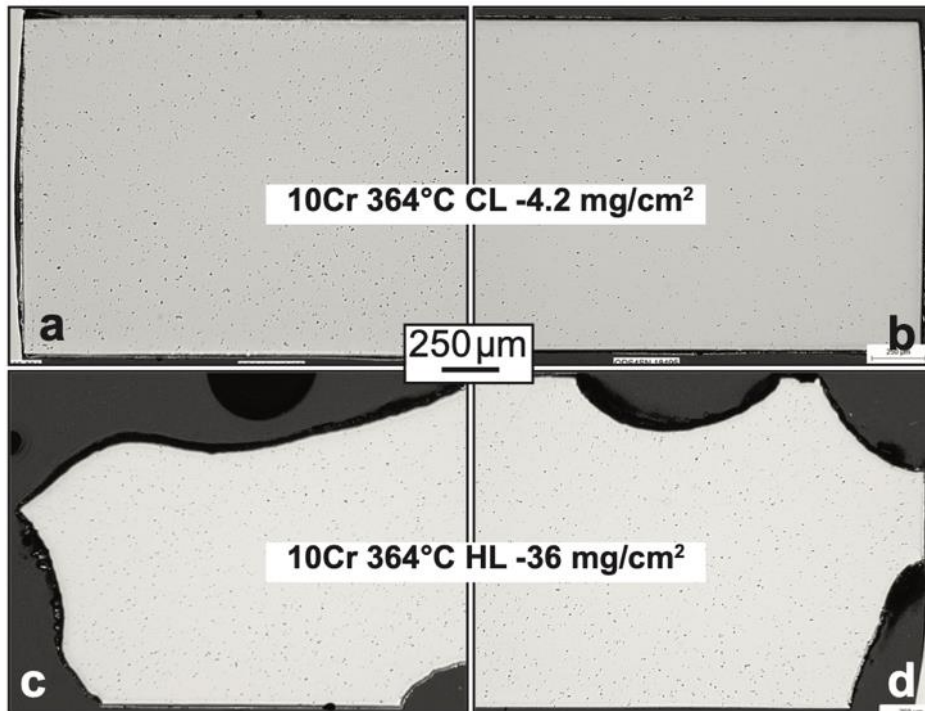
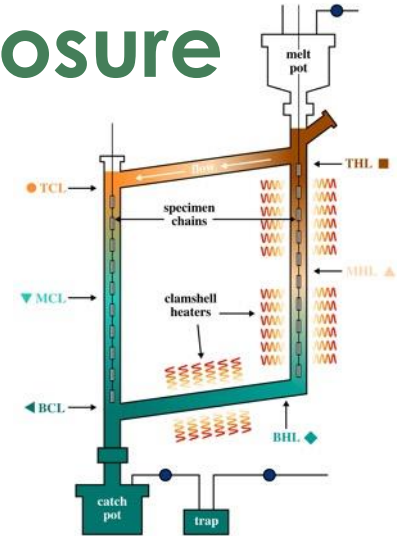
Large mass losses in hot leg for all alloys



# Evidence of pitting on the specimens after Sn exposure



ODS 12Cr  
1mm thick



- It appears that breakdowns in the alumina scale lead to dissolution

# PbLi: expanding on base program foundation

US Base program (started in 2013)

- 3<sup>rd</sup> Pb-Li loop: 650°C peak, APMT monometallic
  - Small mass changes for APMT (Jun et al. JNM 2020)
- 4<sup>th</sup> Pb-Li loop: 700°C peak, APMT monometallic
  - Significant degradation at >675°C (Pint et al. FST 2021)

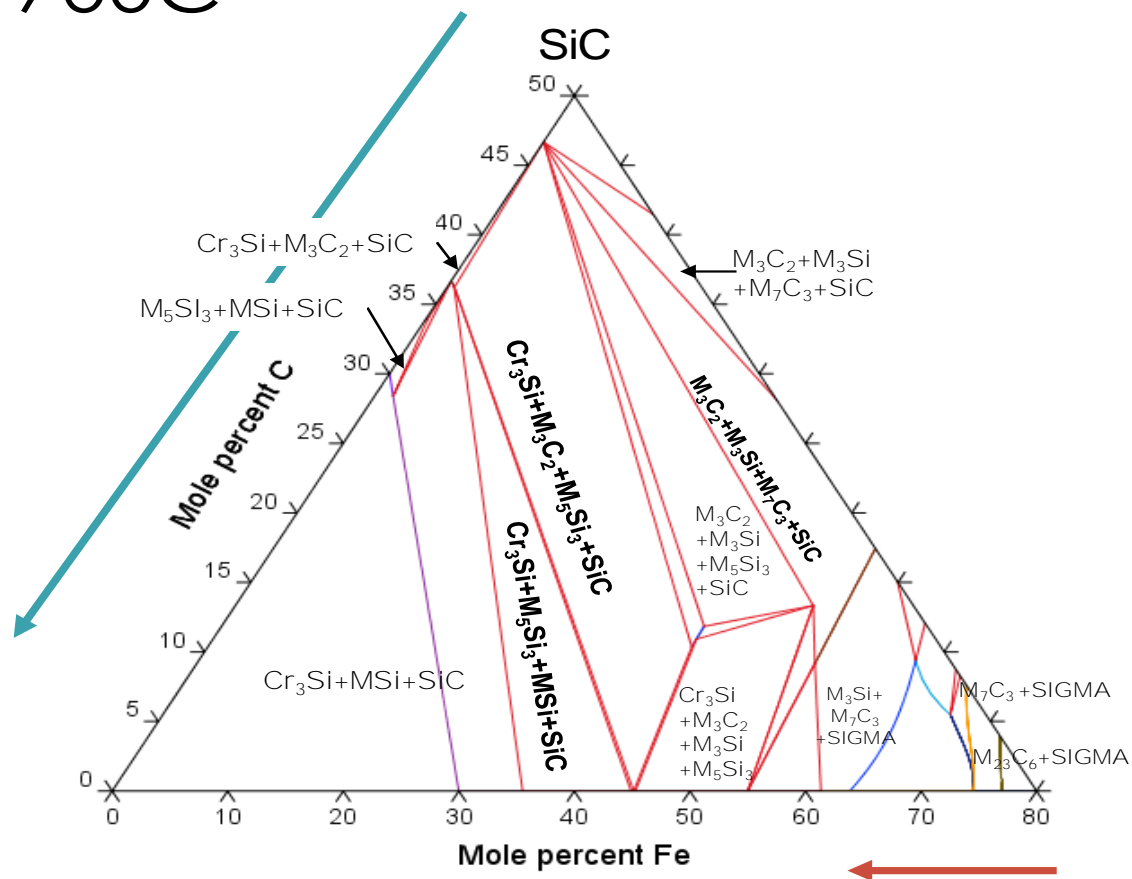
BFC Task 4

- 5<sup>th</sup> Pb-Li loop: 700°C peak, APMT tubing + CVD SiC/ODS FeCrAl
  - Fantastic dissimilar material interaction (Pint et al. FED 2021)
- 6<sup>th</sup> Pb-Li loop: 650°C peak, APMT tubing + SiC/aluminized F82H
  - Completed September 2021 (Romedenne JNM 2023)
- 7<sup>th</sup> Pb-Li loop: 650°C peak, APMT tubing + SiC/aluminized F82H
  - Completed September 2023 (2000 h, study reaction kinetics)



# Thermodynamic modeling of Fe-Si-C-Cr

Fe-Si-C + 20 at% Cr  
700C



Along SiC-C axis: corresponds to SiC-deposit interface

SiC rich region

Most probable phases

- $\text{Cr}_3\text{Si}$
- $\text{M}_3\text{C}_2$  (M=Cr,Fe)
- $\text{MSi}$
- $\text{SiC}$

Along Fe,Cr-SiC interface close to surface  
Fe,Cr rich region

Most probable phases

- $\text{M}_{23}\text{C}_6$
- $\text{M}_7\text{C}_3$
- $\text{M}_3\text{Si}$
- $\text{M}_5\text{Si}_3$
- $\text{Cr}_3\text{Si}$

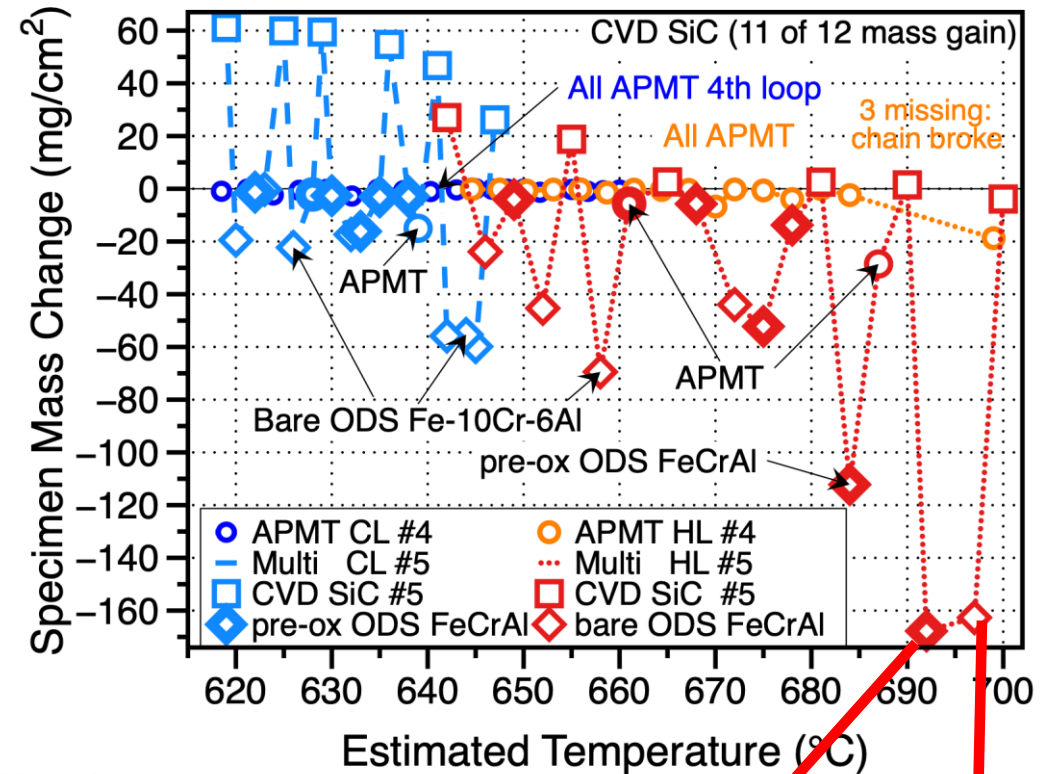
Next: agreement with XRD results!

Pint, Jun and Romedenne, Fusion Engineering Design, 2021

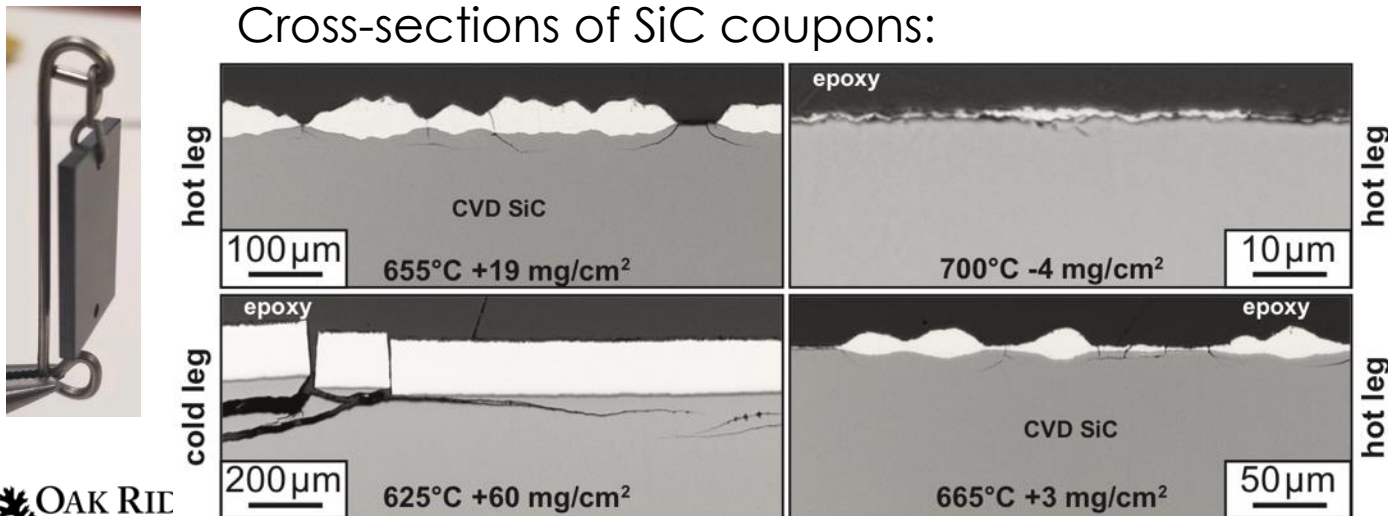
# 5<sup>th</sup> PbLi loop: 'Dissimilar material interaction' between SiC & ODS FeCrAl

- High mass changes in Pb-Li
  - CVD SiC gained mass in cold leg
    - Non-uniform (Fe,Cr) carbides + silicides
    - Reaction with Fe and Cr in Pb-Li
  - Large FeCrAl mass losses
    - Acceleration: Fe/Cr removed from Pb
    - Mistake to not-pre-oxidize all specimens

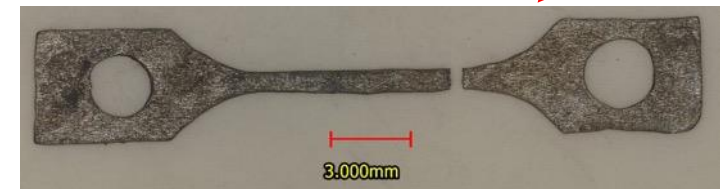
• Conclusion: 700°C is too high!



Cross-sections of SiC coupons:



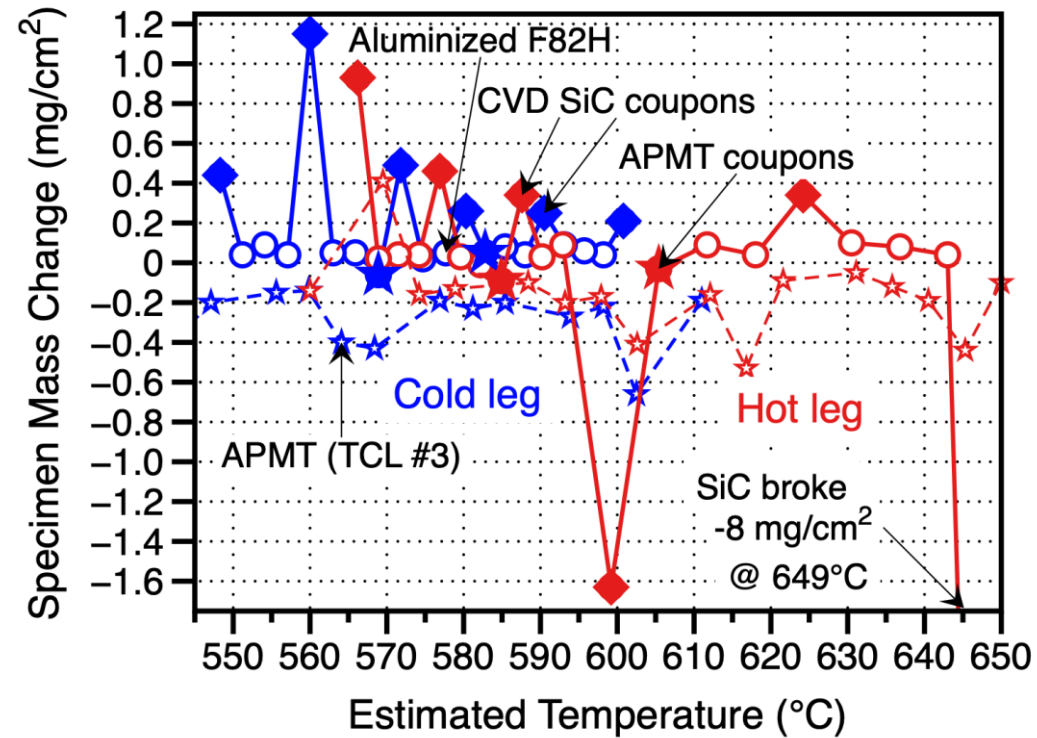
Pre-oxidized ODS FeCrAl



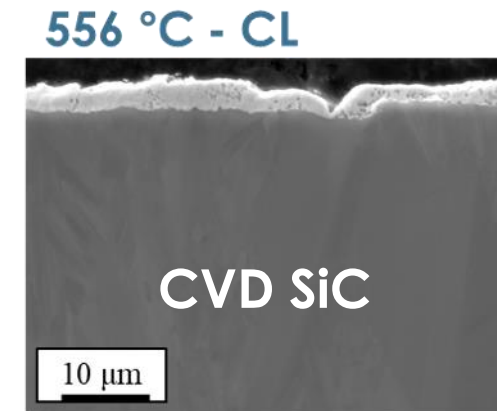
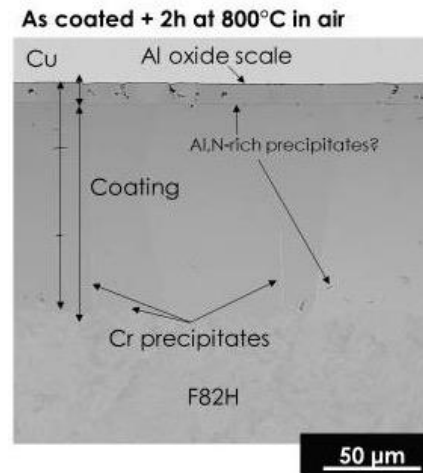
Bare ODS Fe-10Cr-6Al

# #6 650°C: significant reduction in SiC reaction at lower T

- **Aluminized F82H**
  - All pre-oxidized specimens
  - Mostly small mass gains
- **CVD SiC**
  - One broke (-8 mg/cm<sup>2</sup>)
  - 2<sup>nd</sup> may have chipped
  - **10 of 12 mass gain**
    - **Suggests some reaction**
- **APMT coupons**
  - 3 of 4 small mass losses like prior monometallic loop #3

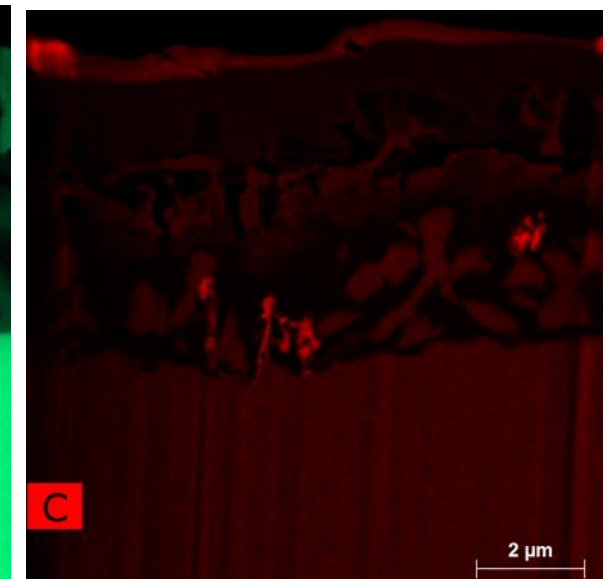
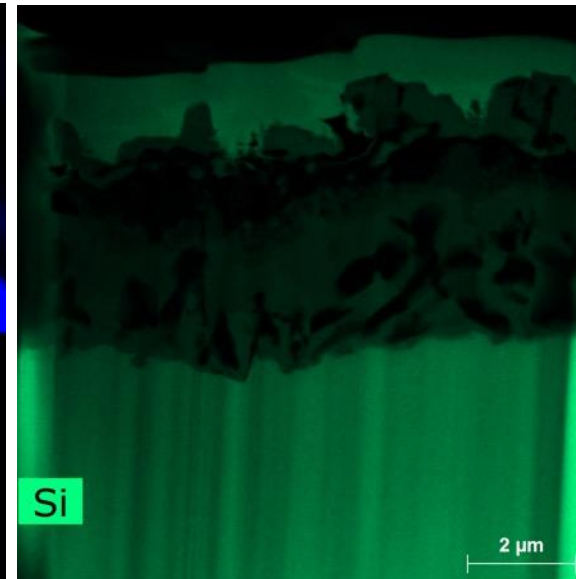
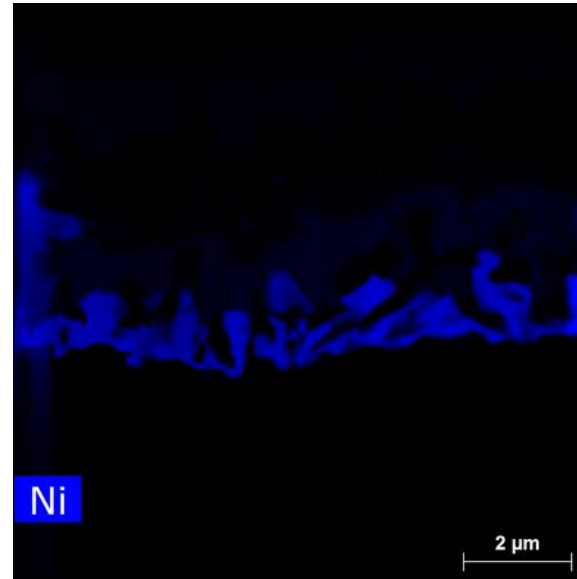
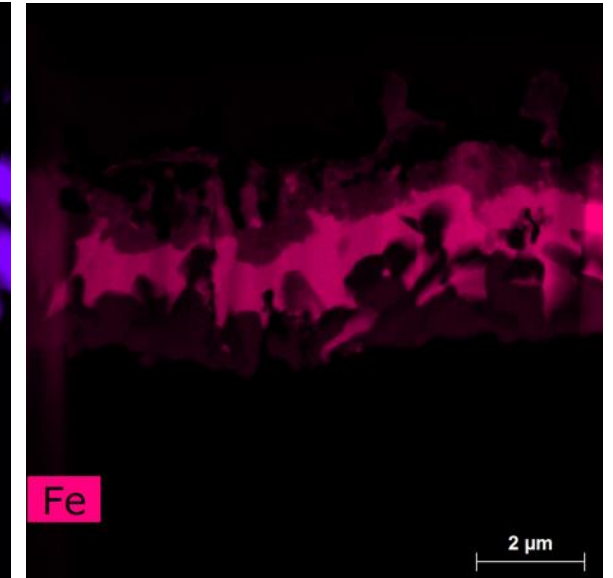
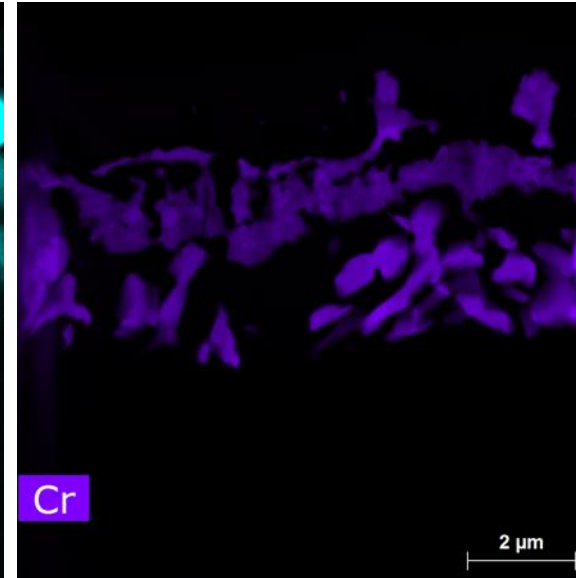
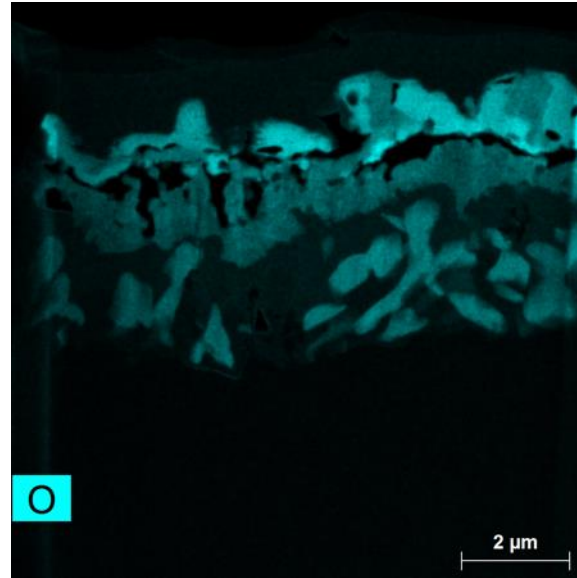
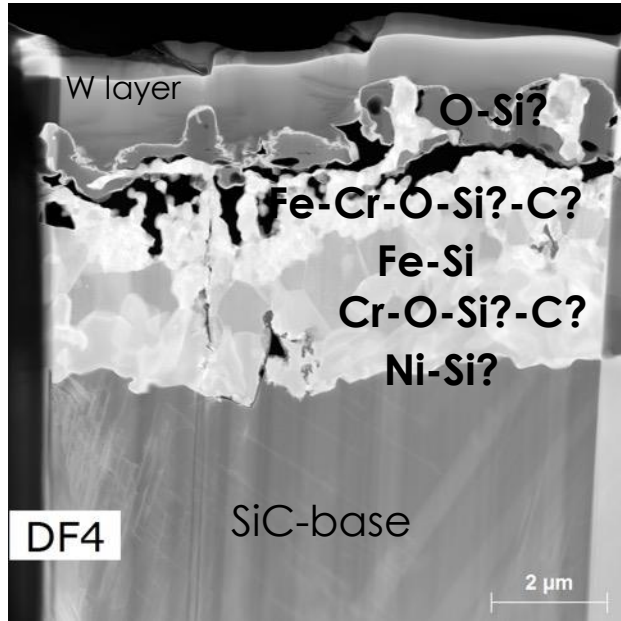


Broken CVD SiC coupon



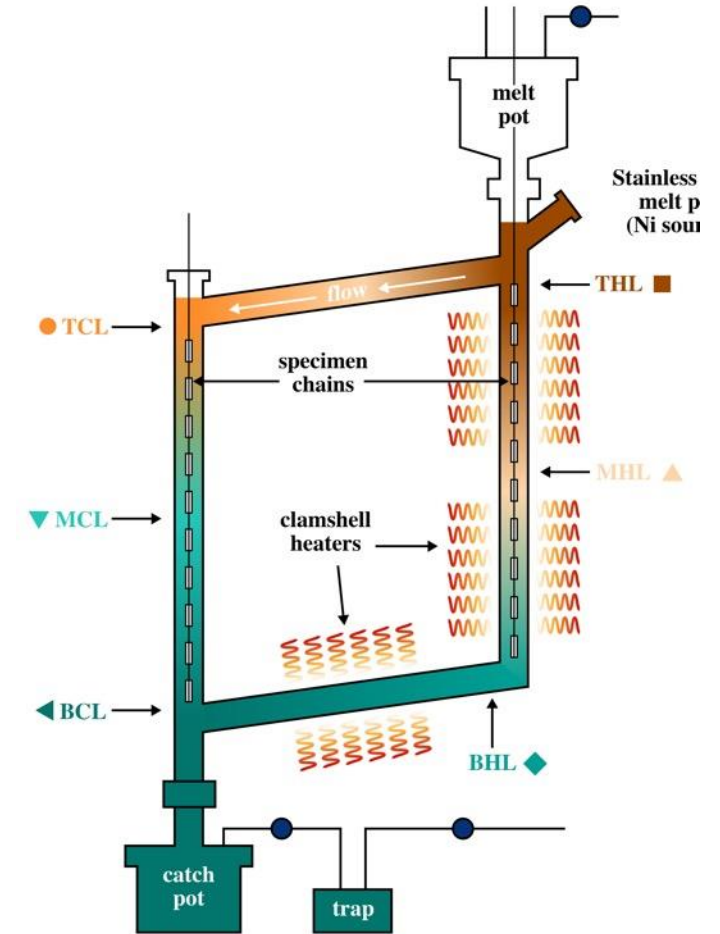
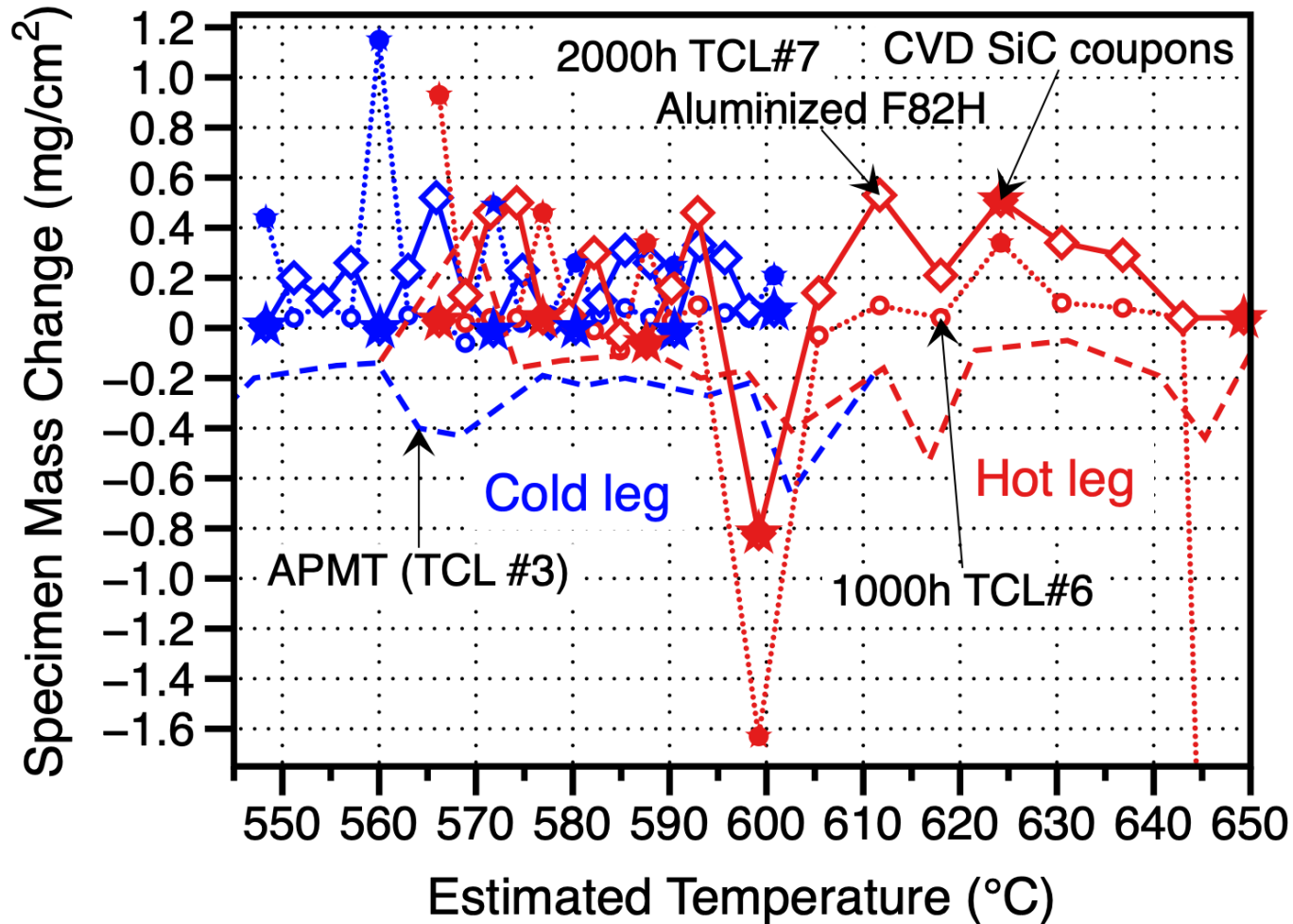
Pack aluminized F82H

# STEM/EDS: maps of reaction product at 566°C (HL)



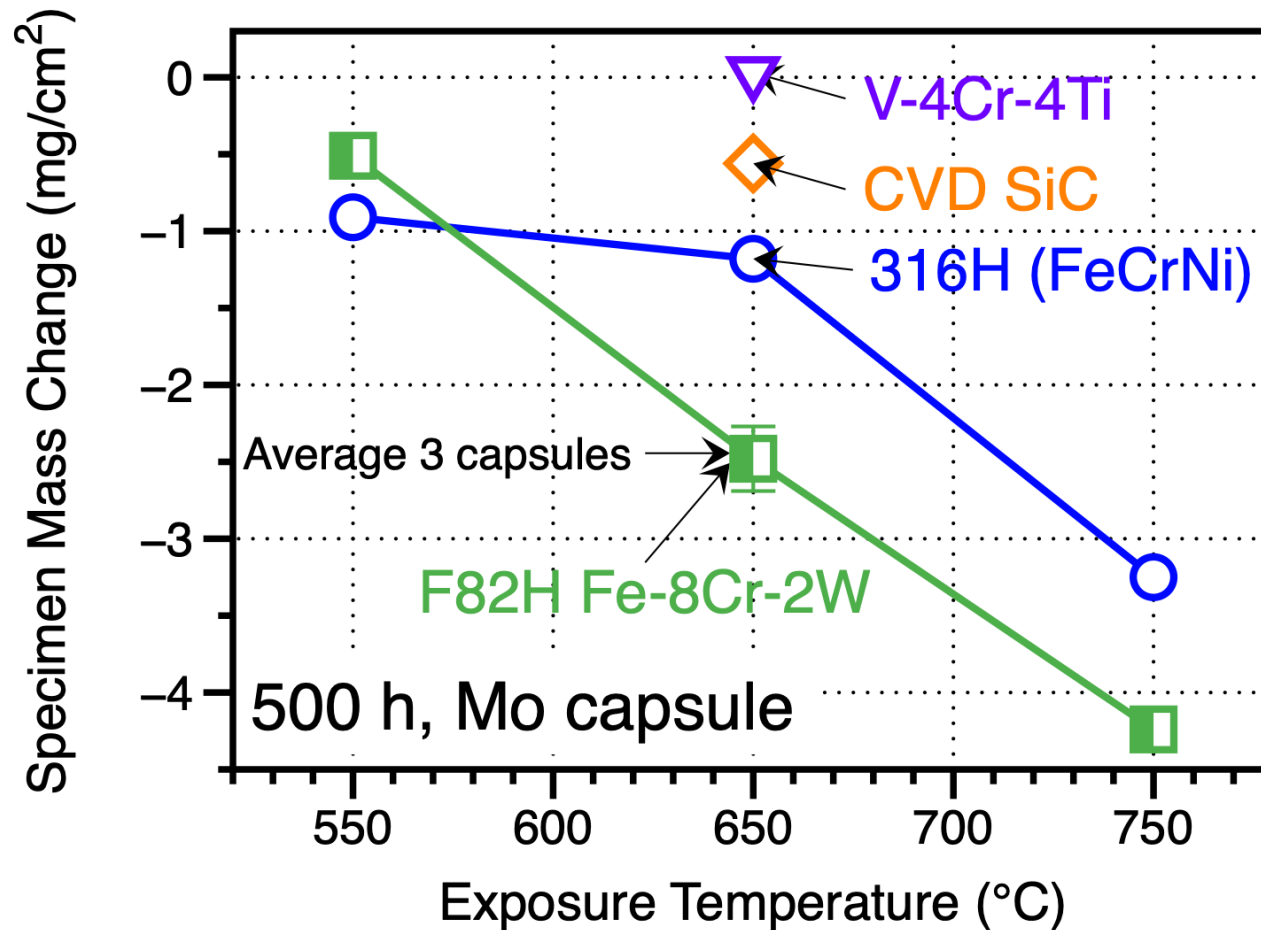
- Complex reaction products, SiC reacting with metals in PbLi: Fe, Cr and Ni?
- Difficult to identify phases

# #7 650°C: just completed 2000 h TCL experiment, similar mass change as 1000 h for aluminized F82H and CVD SiC



Characterization in progress for presentation at ICFRM-21

# Very recent FLiBe results (static commercial FLiBe)



316 outer capsule



FLiBe salt  
specimen

Mo inner capsule

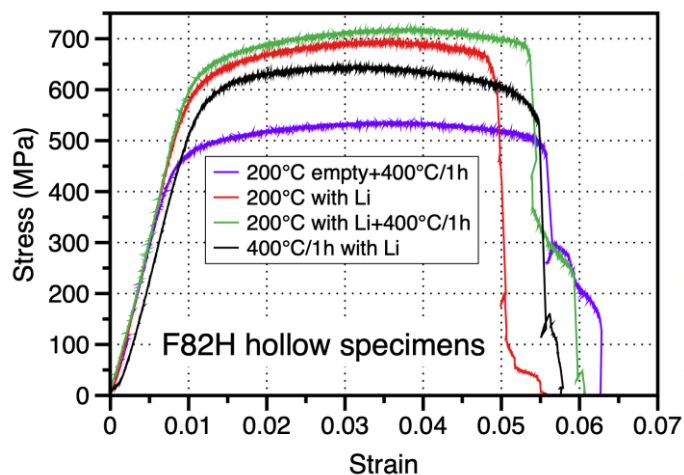
Characterization in progress for presentation at ICFRM-21



# Four different liquid compatibility tasks in progress at ORNL

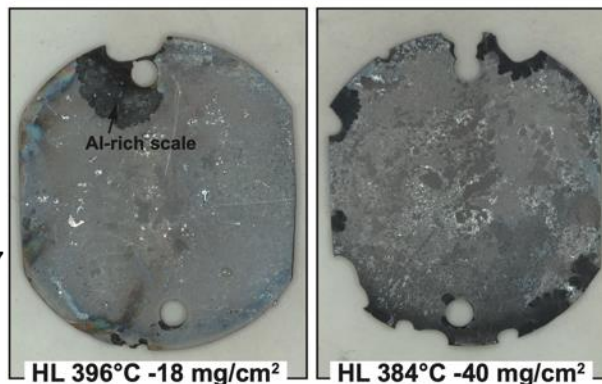
## Plasma Facing Comp. (Li)

- Verified LME in hollow specimens with 4340 steel specimen
- **No significant LME observed for F82H**
  - 200°C tensile/400°C wetting
  - 500°C/500 h anneal



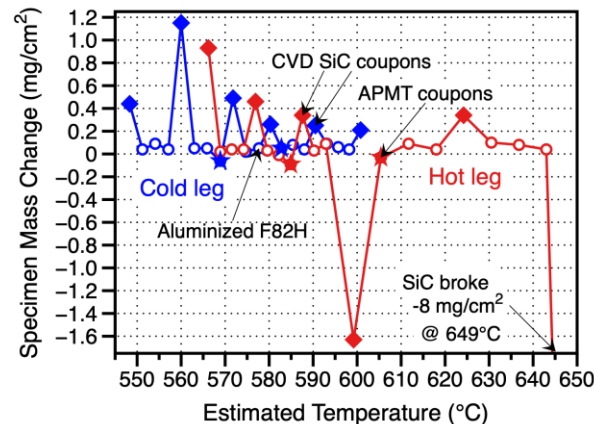
## Sn: FRONTIER Task 3

- Flowing Sn loop showed attack
  - Massive FeCrAl dissolution unlike static tests
  - High hot leg loss
    - Al<sub>2</sub>O<sub>3</sub> not protective
  - **FeCrAl/Sn not viable**
- Complete HFIR irradiation PIE



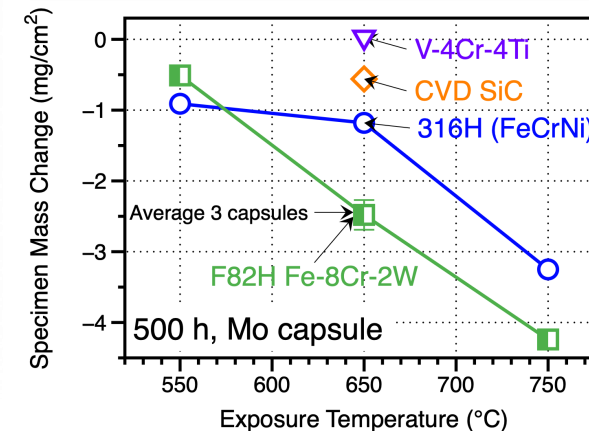
## Blanket (PbLi)

- PbLi loop #5: >675°C massive SiC-FeCrAl interaction
- PbLi loop #6: reduced interaction CVD SiC-aluminize F82H: 650°C
- PbLi loop #7 done:
  - 2000 h, 650°C to study reaction kinetics of SiC in PbLi

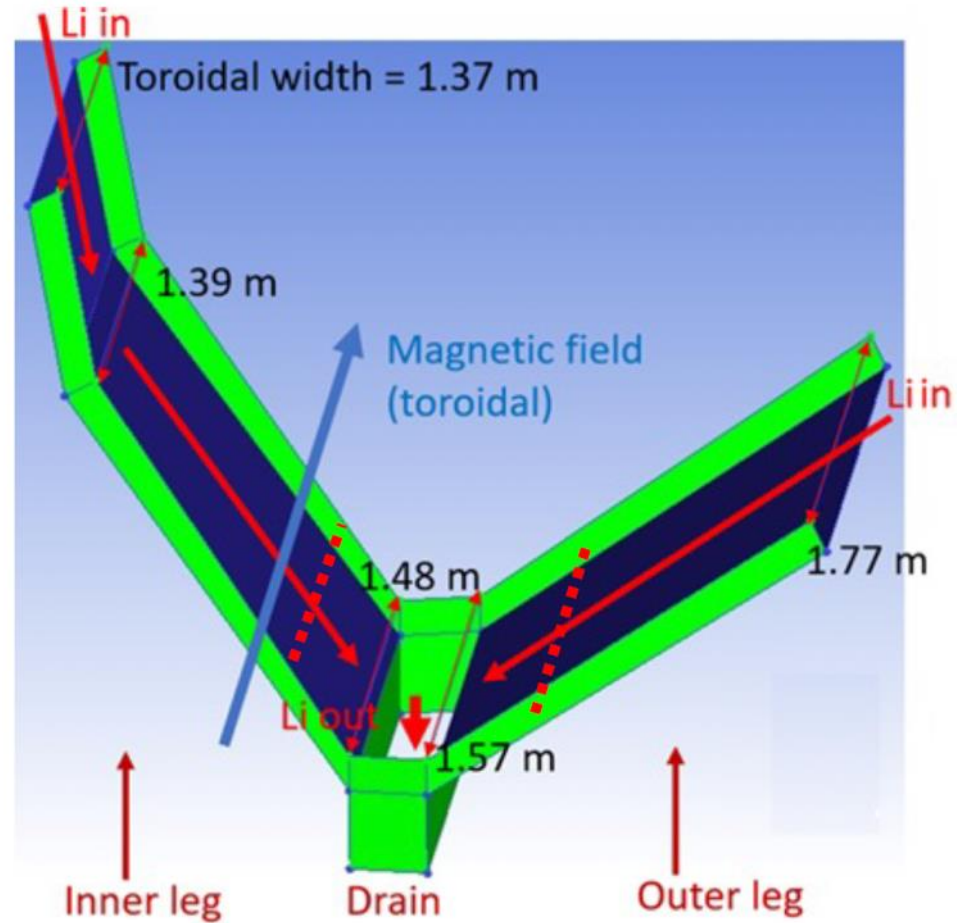


## Blanket (FLiBe)

- Limited FLiBe data
- Initial



# Questions?



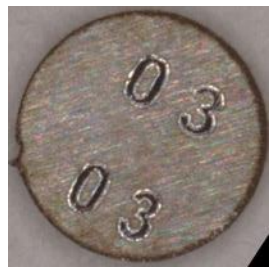
# Frontier Task 3: Flowing Sn test at $\leq 400^\circ\text{C}$ done, HFIR capsules exposed

**Objective:** Evaluate compatibility of flowing Sn with pre-oxidized FeCrAl alloys at  $350^\circ\text{-}400^\circ\text{C}$

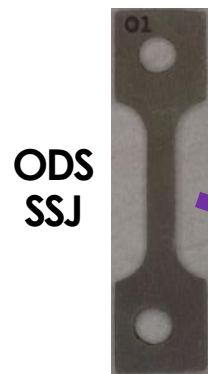
**Approach:** a thermal convection loop (FeCrAlMo alloy APMT) ran 1000 h with 3 alloy specimens: APMT, Japan ODS (12Cr-16Al) and ORNL ODS (10Cr-6Al); all pre-oxidized for 2h at  $1000^\circ\text{C}$  before exposure

**Result:** Pre-oxidation was not sufficient to protect these alloys in these conditions.

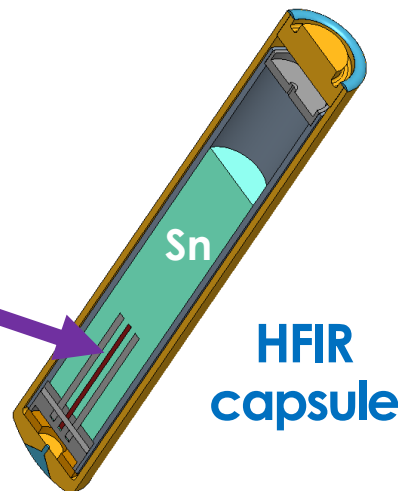
**Next:** HFIR irradiation without Sn (3mm disks) and with Sn (SSJ tensile specimens): **capsules being built for next HFIR cycle**



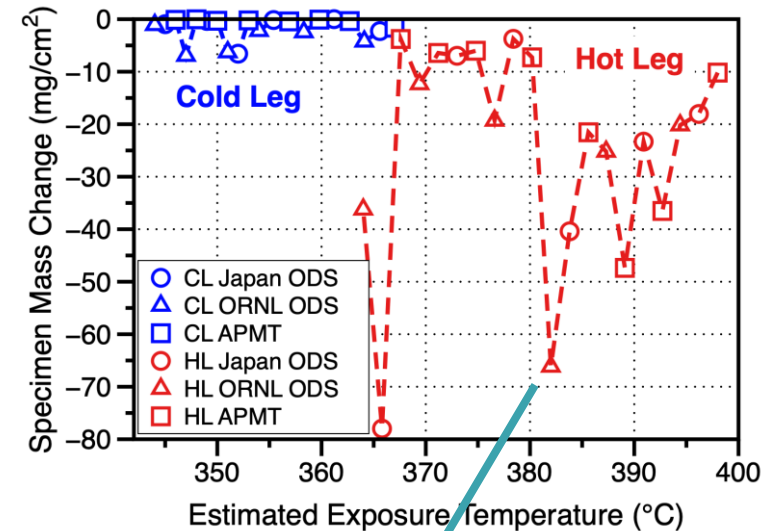
APMT 3 mm disk



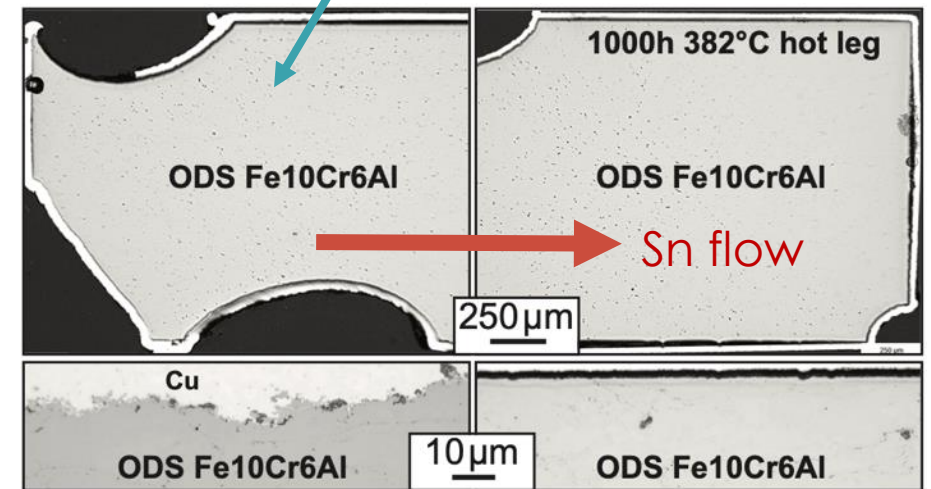
ODS SSJ



HFIR capsule



Mass change data from specimens exposed to flowing Sn for 1,000 h with a peak temperature of  $400^\circ\text{C}$



Light microscopy of ODS FeCrAl after exposure:  
No surface oxide observed in pitted regions