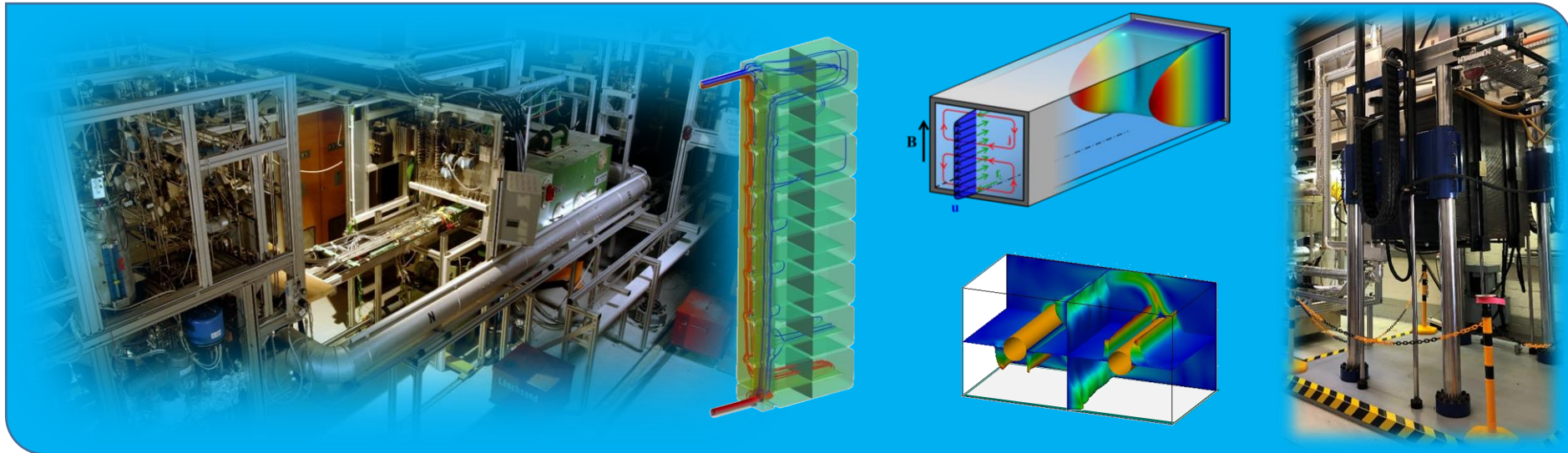


Liquid metal MHD research at KIT

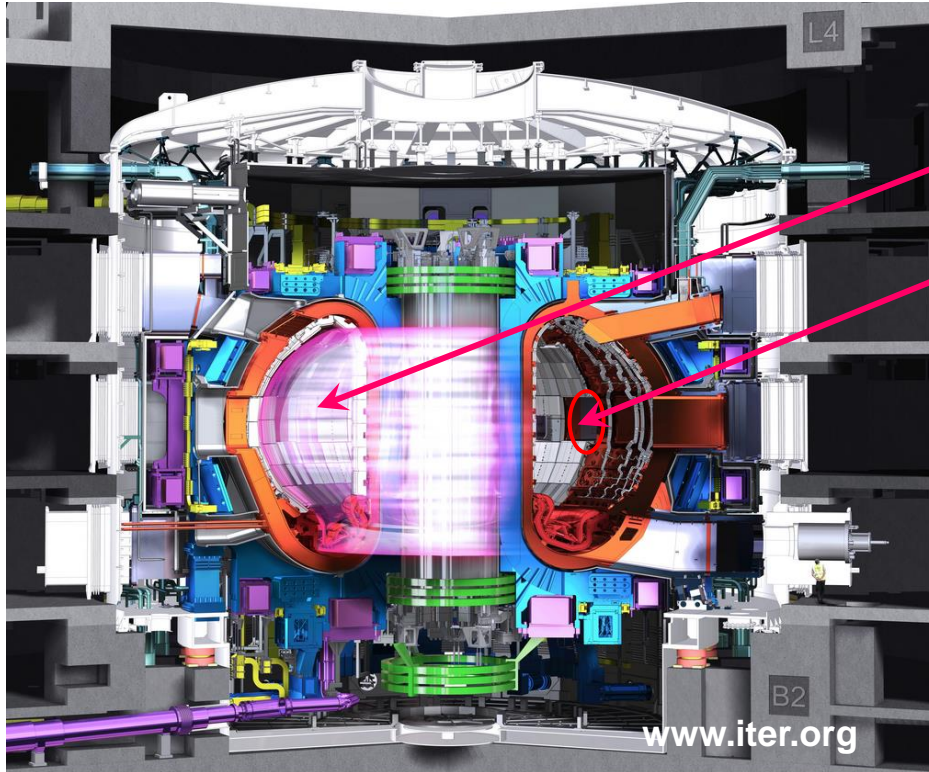
Fundamental phenomena and flows in complex blanket geometries

L. Bühler, and

H. J. Brinkmann, C. Courtessole, V. Klüber, C. Koehly, B. Lyu, C. Mistrangelo, J. Roth



Motivation – applications in nuclear fusion



International Thermonuclear Experimental Reactor ITER

Fusion plasma in magnetic confinement

Blankets around plasma

- shielding of radiation
- breeding of tritium
- conversion of nuclear power
- heat removal

with liquid metal PbLi as breeder and coolant

Magnetohydrodynamics (MHD)

Motivation

Liquid metal magnetohydrodynamic (MHD) flows

- ❑ phenomena
- ❑ equations and parameters

MHD research at Karlsruhe Institute of Technology KIT

- ❑ facilities MEKKA and MaPLE supporting theoretical analyses

Some results

- ❑ duct or pipe flow
 - ❑ applied example, technological development
 - ❑ fundamental research
- ❑ Work related WCLL blankets
 - ❑ basic research
 - ❑ blanket engineering

Overview

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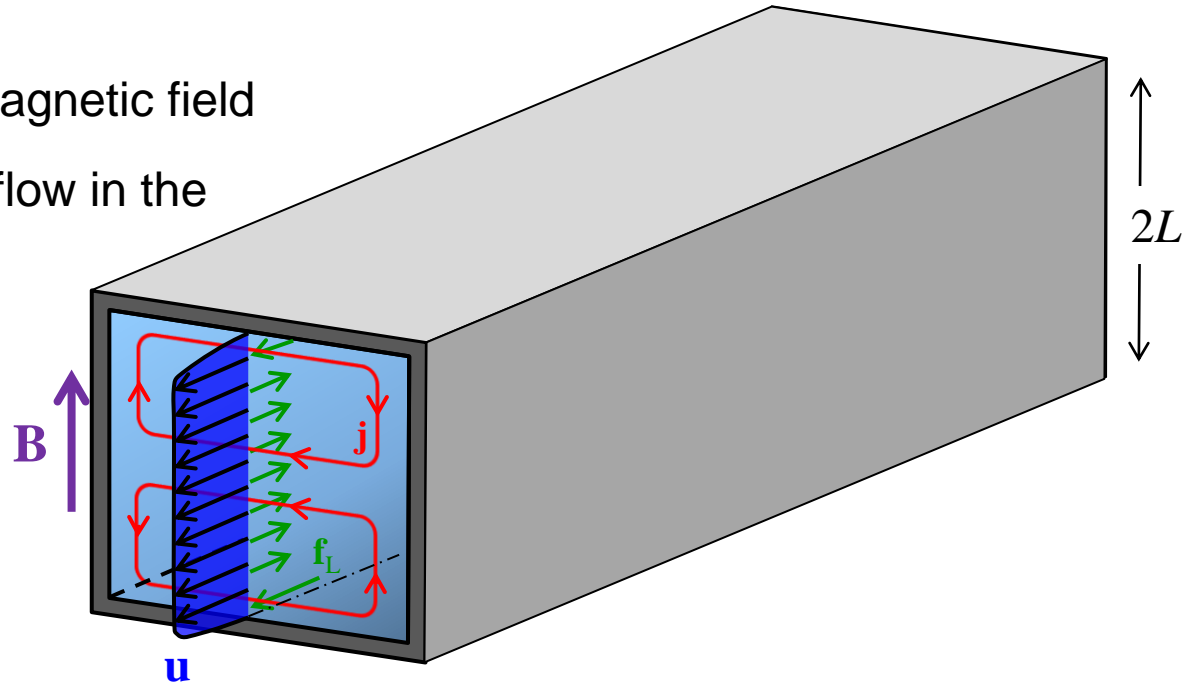
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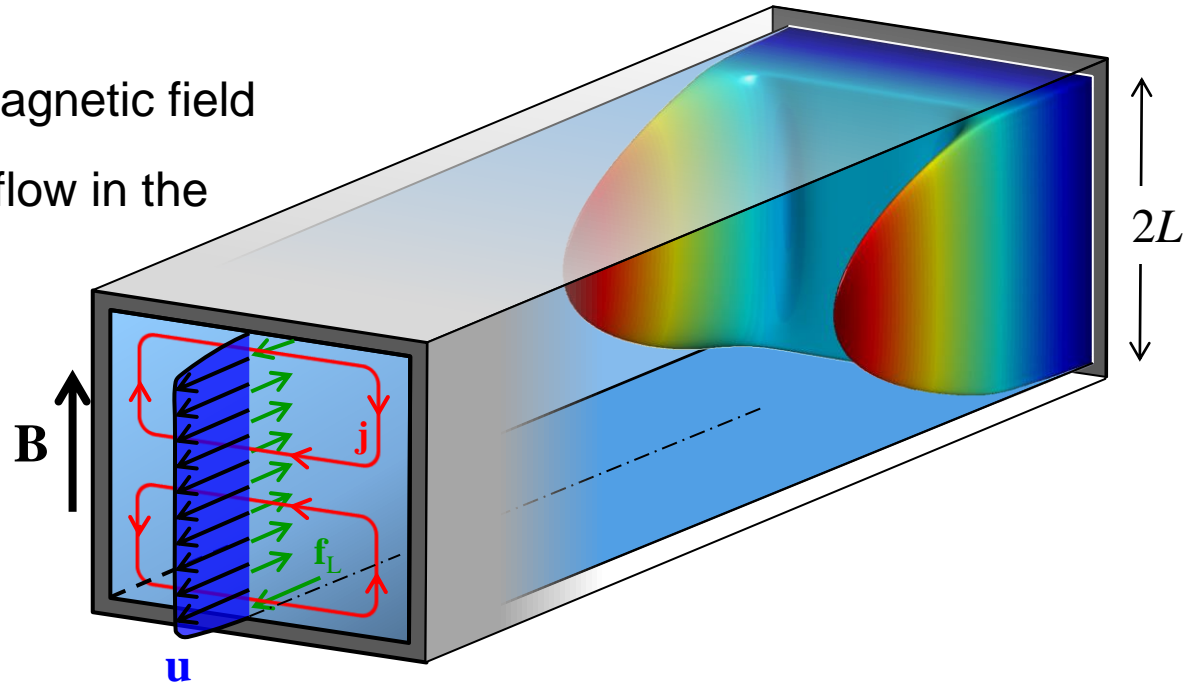
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- ❑ Liquid metal flow in a duct
- ❑ Flow-induced currents in magnetic field
- ❑ Lorentz force opposes the flow in the core \rightarrow large Δp



- ❑ Liquid metal flow in a duct
- ❑ Flow-induced currents in magnetic field
- ❑ Lorentz force opposes the flow in the core \rightarrow large Δp
- ❑ Strange velocity profiles
 - ❑ uniform core
 - ❑ thin boundary layers
 - ❑ jets on side walls possible



Governing equations

Momentum

$$\rho(\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u}) = -\nabla p + \rho \nu \nabla^2 \mathbf{u} + \mathbf{j} \times \mathbf{B}$$

← Lorentz force \mathbf{f}_L

Mass conservation

$$\nabla \cdot \mathbf{u} = 0$$

← flow-induced electric field

Ohm's law

$$\mathbf{j} / \sigma = -\nabla \phi + \mathbf{u} \times \mathbf{B}$$

Charge conservation

$$\nabla \cdot \mathbf{j} = 0$$

→ with proper scales for length L , velocity U , magnetic field B_0

Governing equations, nondimensional

Momentum $\frac{1}{N} (\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u}) = -\nabla p + \frac{1}{Ha^2} \nabla^2 \mathbf{u} + \mathbf{j} \times \mathbf{B}$

Mass conservation $\nabla \cdot \mathbf{u} = 0$

Ohm's law $\mathbf{j} = -\nabla \phi + \mathbf{u} \times \mathbf{B}$

Charge conservation $\nabla \cdot \mathbf{j} = 0$

Parameters

Interaction parameter $N = \frac{\sigma L B_0^2}{\rho U}$

Hartmann number $Ha = LB_0 \sqrt{\frac{\sigma}{\rho \nu}}$

Parameters in fusion

Interaction parameter $N = \frac{\sigma L B_0^2}{\rho U} = \frac{\text{electromagnetic force}}{\text{inertia force}} \approx 10^3 - 2 \times 10^5$ *)

Hartmann number $Ha = L B_0 \sqrt{\frac{\sigma}{\rho \nu}} = \sqrt{\frac{\text{electromagnetic force}}{\text{viscous force}}} \approx 6 \times 10^3 - 3 \times 10^4$ *)

→ electromagnetic force is dominant !!

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MHD platform at KIT: MEKKA & MaPLE

- ❑ **MEKKA and MaPLE are unique and complementary facilities** for addressing MHD challenges for liquid metal blankets
 - ❑ fusion relevant MHD parameter range
 - ❑ big experimental volume for complex geometries
 - ❑ experiments for combined MHD and buoyancy effects

- ❑ **Fundamental experiments in generic geometries for**
 - ❑ improving the understanding of coupled multiphysics phenomena
 - ❑ provide insight for blanket designers

- ❑ **Development of predictive tools and validation**
 - ❑ extension of benchmark database by experiments

- ❑ **Technological development under prototypical conditions**
 - ❑ test measuring techniques
 - ❑ development and test of insulating flow channel inserts (FCI), etc.

- ❑ **Validation of design concepts for liquid metal blankets (mock-up tests)**

MEKKA

Magnetohydrodynamische Experimente mit Natrium Kalium Karlsruhe



Liquid metal loop

- ❑ Model fluid: eutectic sodium-potassium ($Na_{22}K_{78}$ used as model fluid)
- ❑ Inventory 200 l, pump (9 bar, 25 m³/h), thermostat, instrumentation, ...
- ❑ Advantage of NaK : operate at room temperature
 - thermoelectric perturbations are minimized → highly accurate results
 - high (σ/ρ) → fusion relevant parameters at available magn. field

Parameters

Interaction parameter

$$N = \frac{\sigma}{\rho} \frac{LB_0^2}{U}$$

Hartmann number

$$Ha = LB_0 \sqrt{\frac{\sigma}{\rho \nu}}$$

Liquid metal loop

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Big dipole magnet

- ❑ Maximum field: 2.1 T
- ❑ Large volume of uniform magnetic field: 800 × 480 × 165 mm³
 - experiments in large and complex geometries such as blanket mock-ups

MaPLE

Magnetohydrodynamic PbLi Experiments

MaPLE

- ❑ **Built and first operated at UCLA**
 - PbLi flows under transverse magnetic field (prototypical fluid)
- ❑ **Upgraded with EUROfusion**
 - for combined MHD and buoyancy effects
- ❑ **Main components**
 - PbLi loop (up to 450°C), storage tank (70 l), pump (6 bar, 7.2 m³/h), air cooler (70 kW),



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 - PbLi loop (up to 450°C), storage tank (70 l), pump (6 bar, 7.2 m³/h), air cooler (70 kW),
 - Dipole magnet (20 ton, 2 T) with hydraulic positioning frame for various orientations



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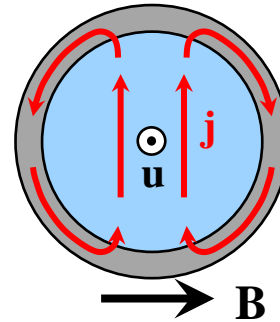
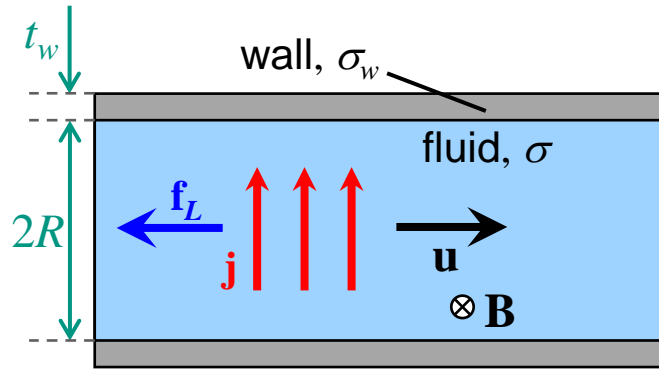
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Insulating Flow Channel Inserts FCIs for pressure drop reduction

MHD flows in conducting and insulating pipes



Currents find shortcut through walls

→ high current density j

→ strong Lorentz force f_L

→ large pressure drop $\nabla p \propto \sigma U B_0^2$

Chang & Lundgren, 1961; Miyazaki et al., 1983

Example in fusion (PbLi pipe flow: $R=0.1\text{m}$, $U=0.1\text{m/s}$, $B=4\text{T}$, → $Ha \approx 9000$)

perfectly conducting wall

$$\frac{\partial p}{\partial x} \approx 14 \frac{\text{bar}}{\text{m}}$$

thin wall, $t_w/R=0.2$

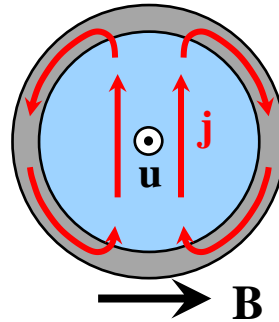
$$\frac{\partial p}{\partial x} \approx 3 \frac{\text{bar}}{\text{m}}$$

insulating wall

$$\frac{\partial p}{\partial x} \approx 2 \times 10^{-3} \frac{\text{bar}}{\text{m}}$$

→ insulation is a key for good MHD performance

MHD flows in conducting and insulating pipes

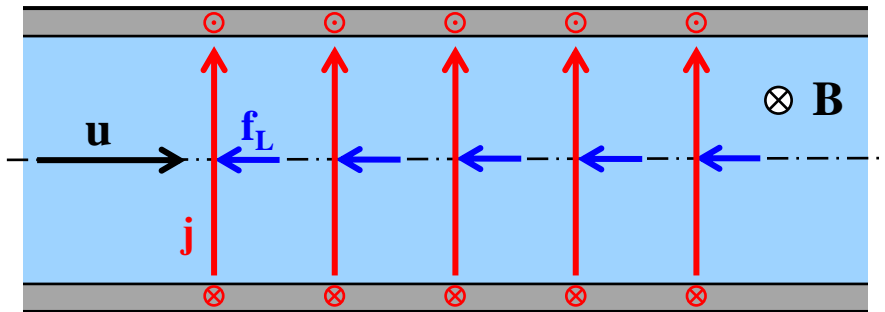


Currents find shortcut through walls

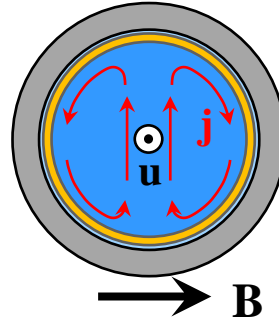
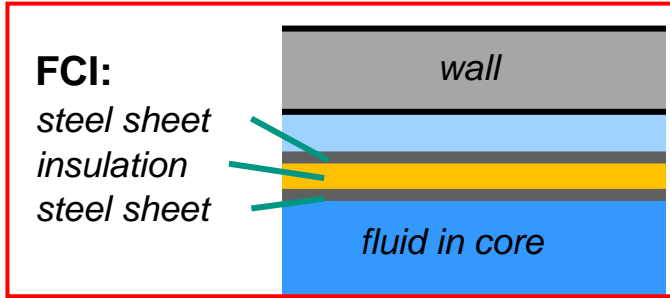
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MHD flows in conducting and insulating pipes

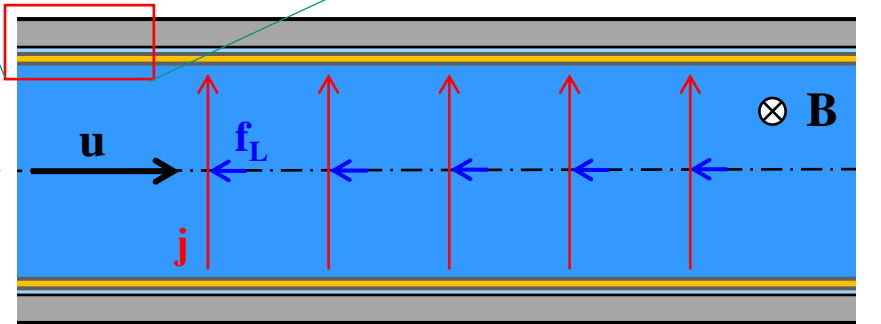


Sandwich – type FCI

- insulation is protected by thin sheets
 - FCI fabricated and tested at KIT
- Koehly et al. Fusion Science and Technology, 2017, 72, 660*

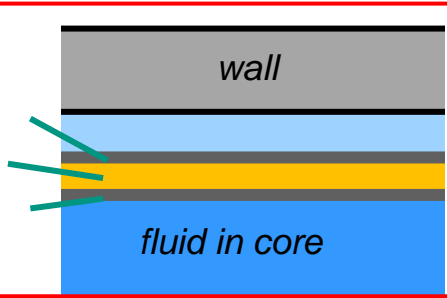
Insulating Flow Channel Inserts (FCI)

- interrupt currents into the wall
- reduce pressure drop



FCI:

steel sheet
insulation
steel sheet

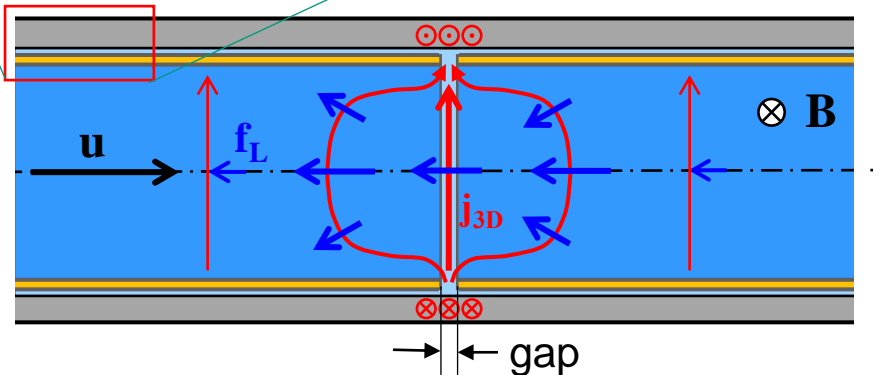


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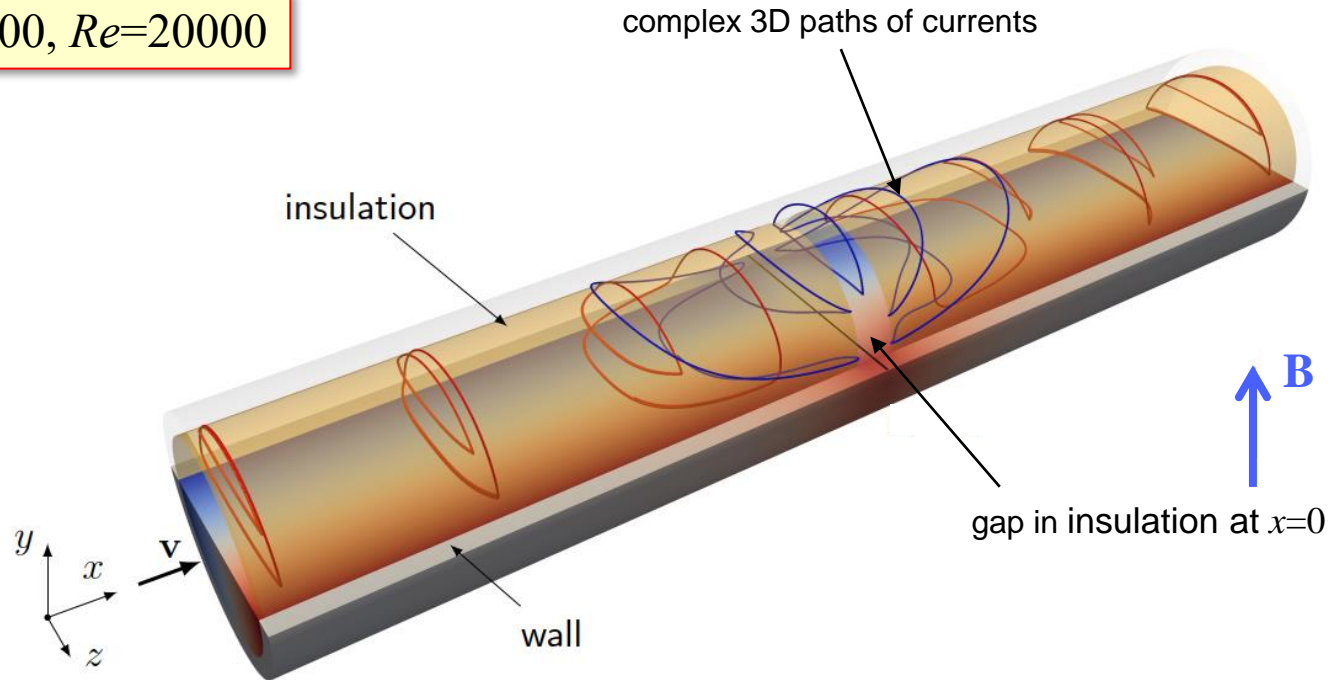
Insulating Flow Channel Inserts (FCI)

- interrupt currents into the wall
- reduce pressure drop
- **gaps between two FCI**
 - local leakage currents j_{3D}
 - strong local 3D effects



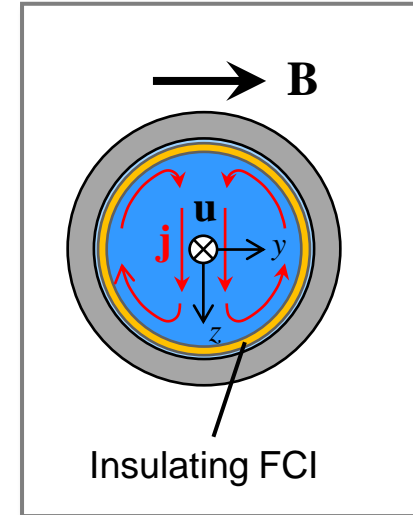
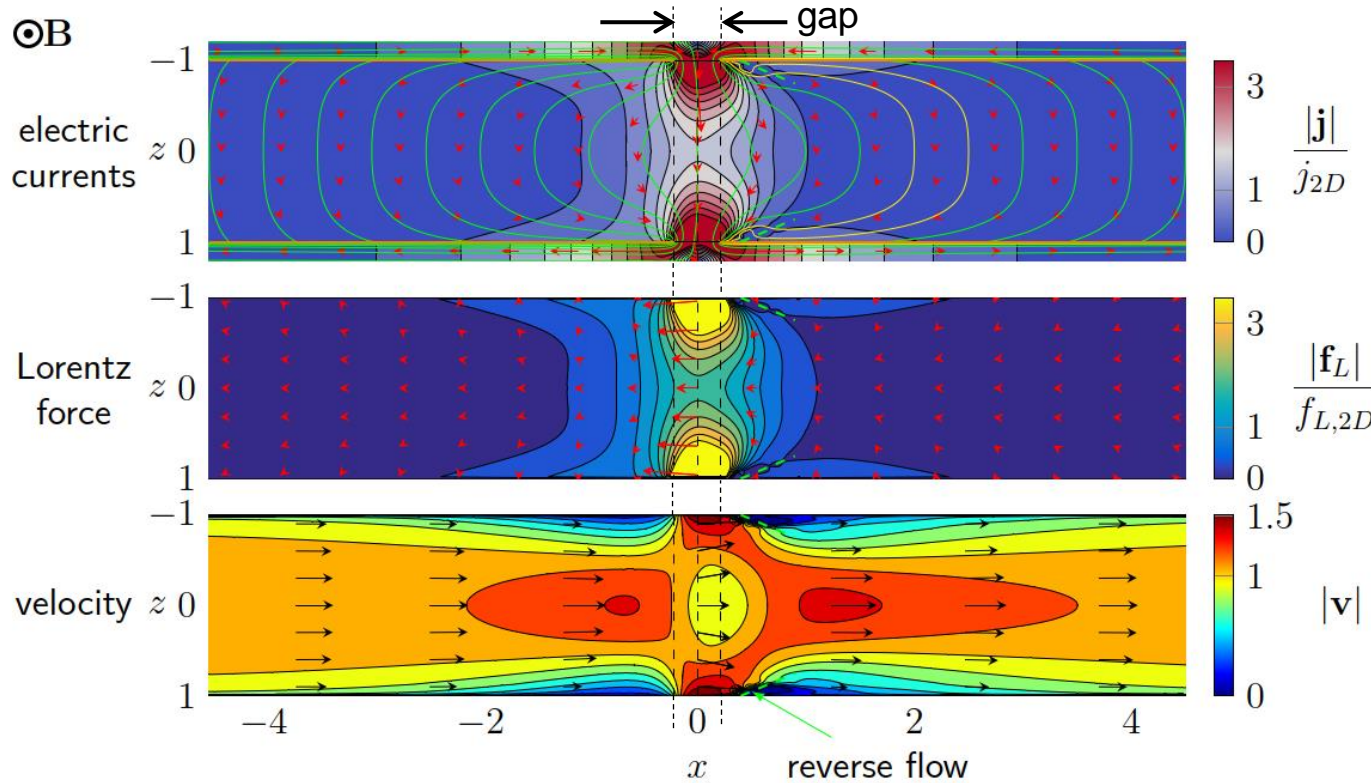
3D effects at gaps between two FCIs

$Ha=2000, Re=20000$



Electric currents and potential near an axial gap between two FCIs

3D effects at gaps between two FCIs

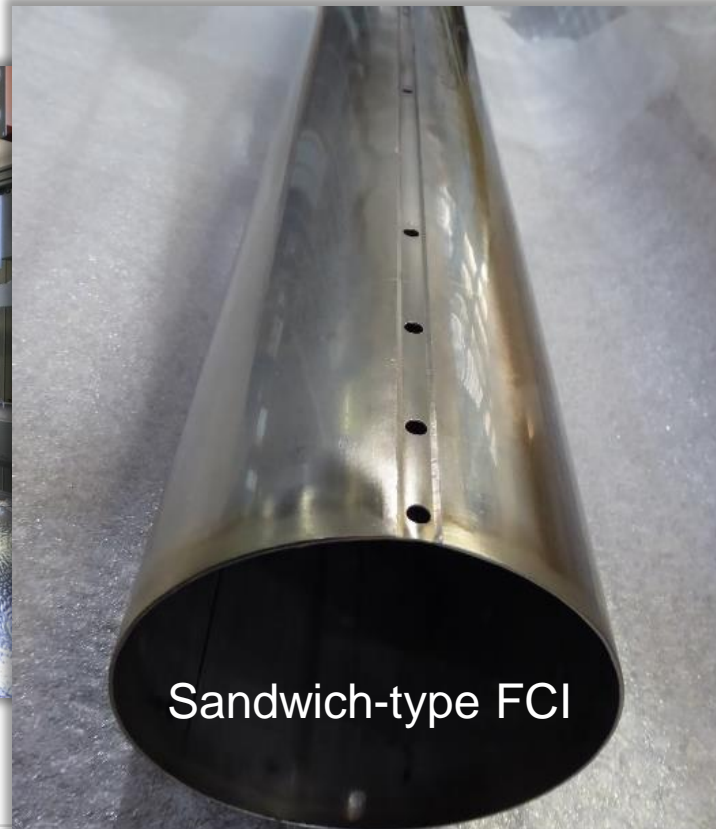


Flow properties in horizontal symmetry plane $y = 0$

Gaps between two FCIs, experiments in MEKKA



Installed in MEKKA loop



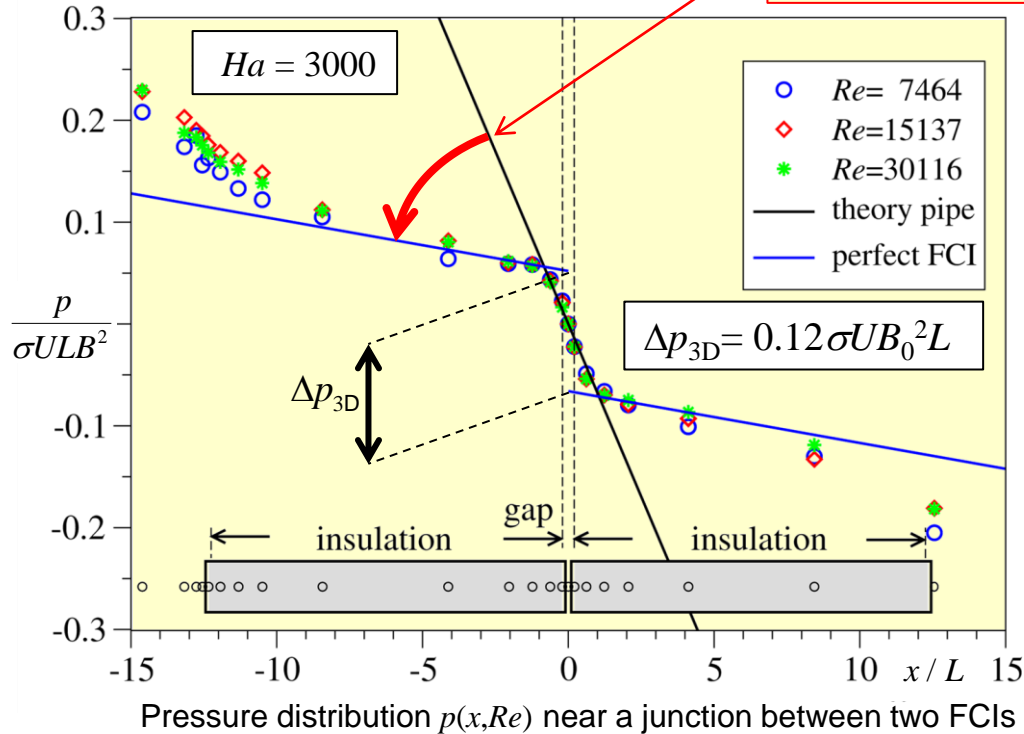
Sandwich-type FCI



Instrumented test section

Gaps between two FCIs, experiments in MEKKA

Experimental data



Experiments confirm

- reduction of pressure gradient for fully developed flow by a factor 13
- 3D effects near gap between FCIs
- locally increased pressure drop Δp_{3D}
- scaling law for Δp_{3D} confirmed for a wide range of Re and Ha

Overview

Motivation


Liquid metal magnetohydrodynamic (MHD) flows

- ❑ phenomena
- ❑ equations and parameters

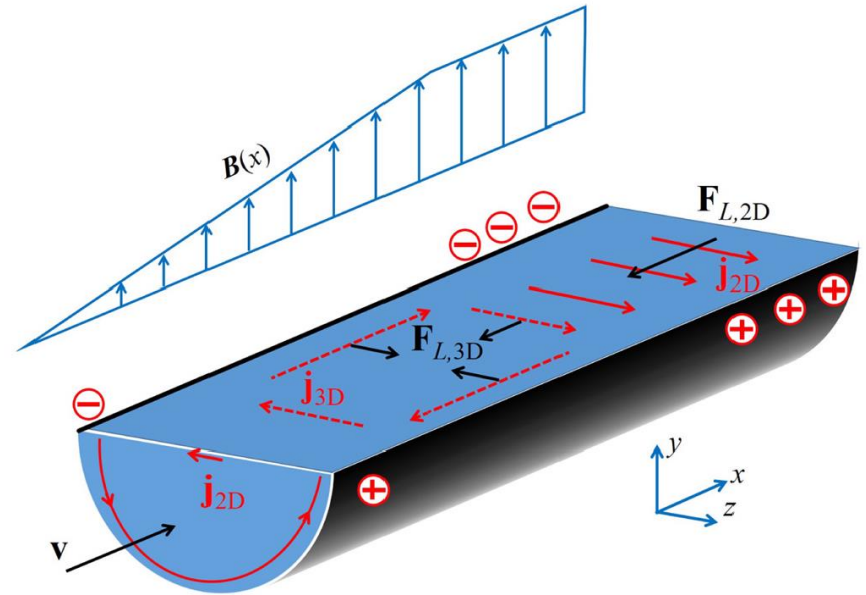
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Some results

- ❑ **duct or pipe flow**
 - ❑ applied example, technological development
 - ❑ **fundamental MHD problem** 
- ❑ Work related WCLL blankets
 - ❑ basic research
 - ❑ blanket engineering

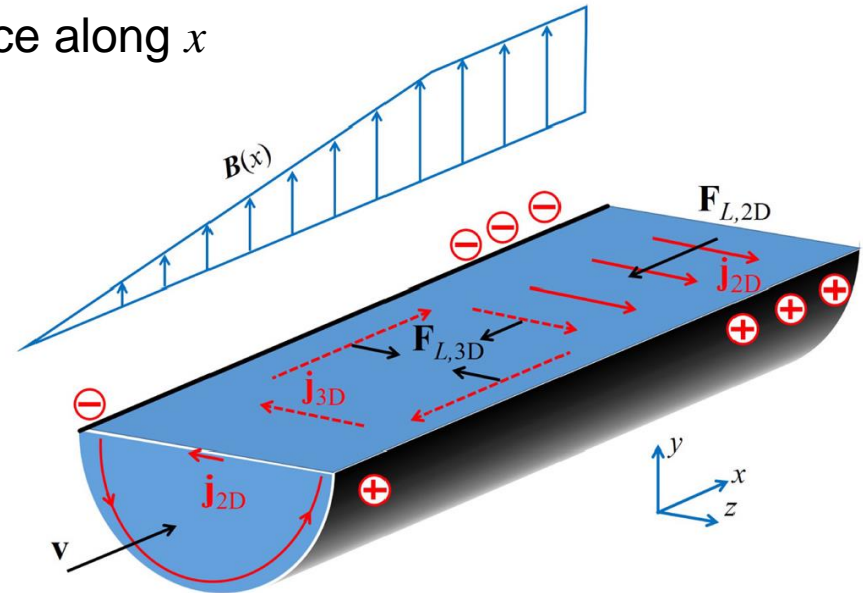
MHD flow in a non-uniform magnetic field $B(x)$



Flow in non-uniform B-field

Flow into a magnet

- turbulent flow at high Re entering a magnet
- increasing transverse potential difference along x
 - 3D current loops
 - extra Lorentz forces

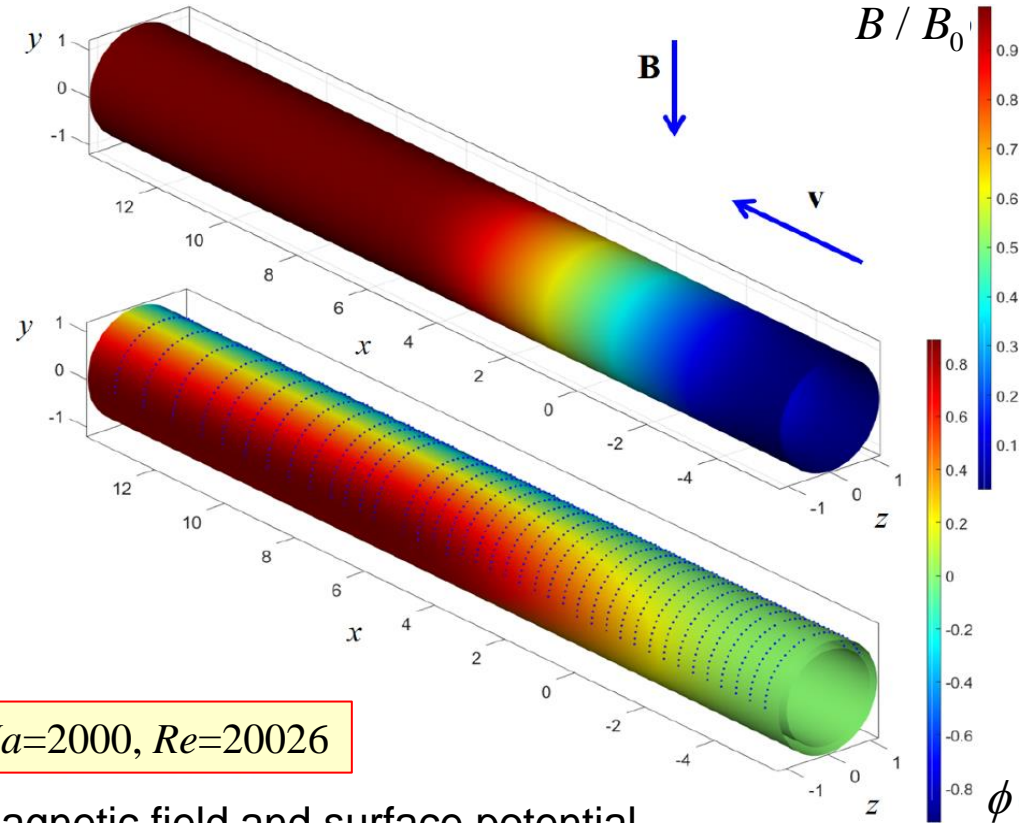


Flow in non-uniform

Flow into a magnet

- turbulent flow at high Re enters
- increasing transverse potential
→ 3D current loops
→ extra Lorentz forces
- experiments
→ yield potential data on surface

MEKKA experiment at KIT



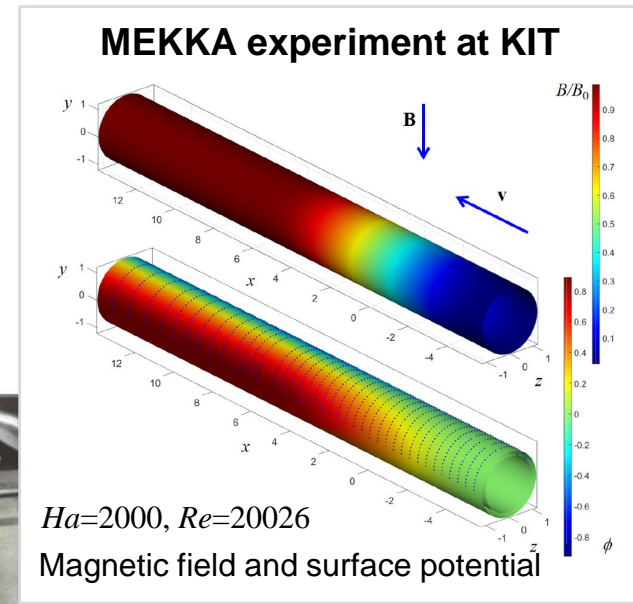
$Ha=2000, Re=20026$

Magnetic field and surface potential

Flow in non-uniform B-field

Flow into a magnet

- turbulent flow at high Re entering a magnet
- increasing transverse potential difference along x
 - 3D current loops
 - extra Lorentz forces
- experiments
 - yield potential data on surface
- asymptotic theory
 - reconstruction of 3D velocity from measured surface data

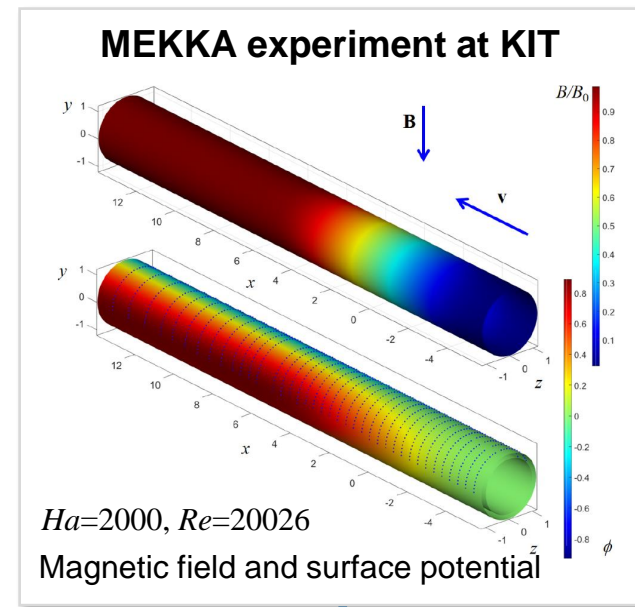
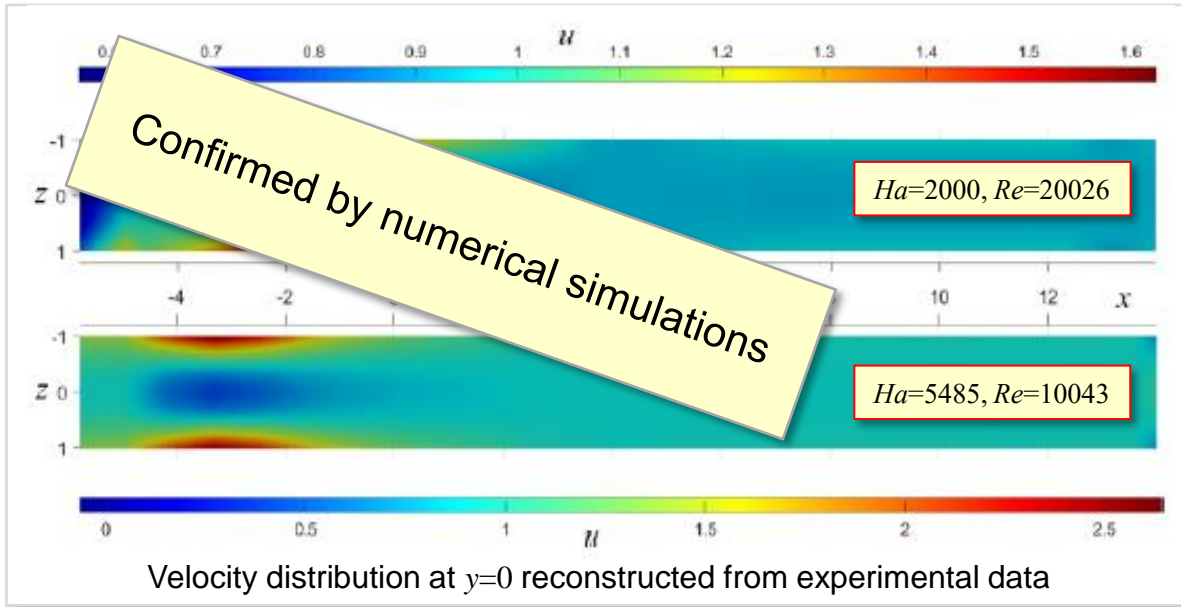


$$u(y, z) \approx B^{-1} \frac{\partial \phi}{\partial z}$$

Flow in non-uniform B-field

near entrance to B-field

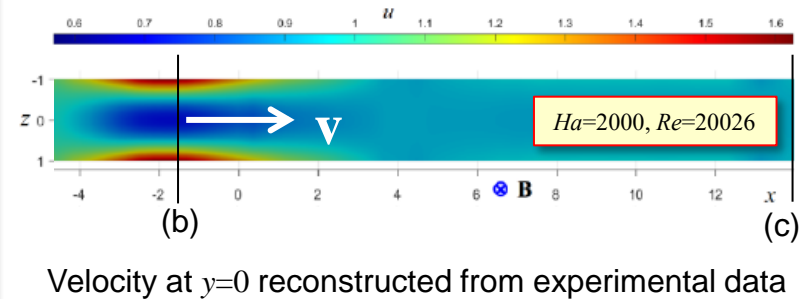
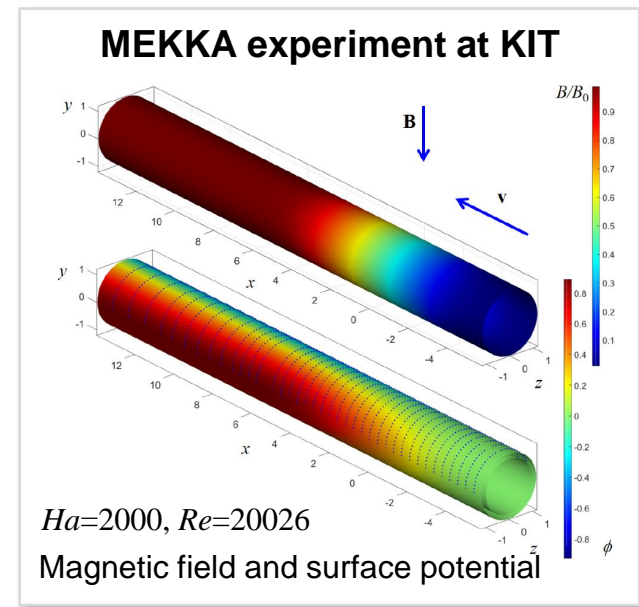
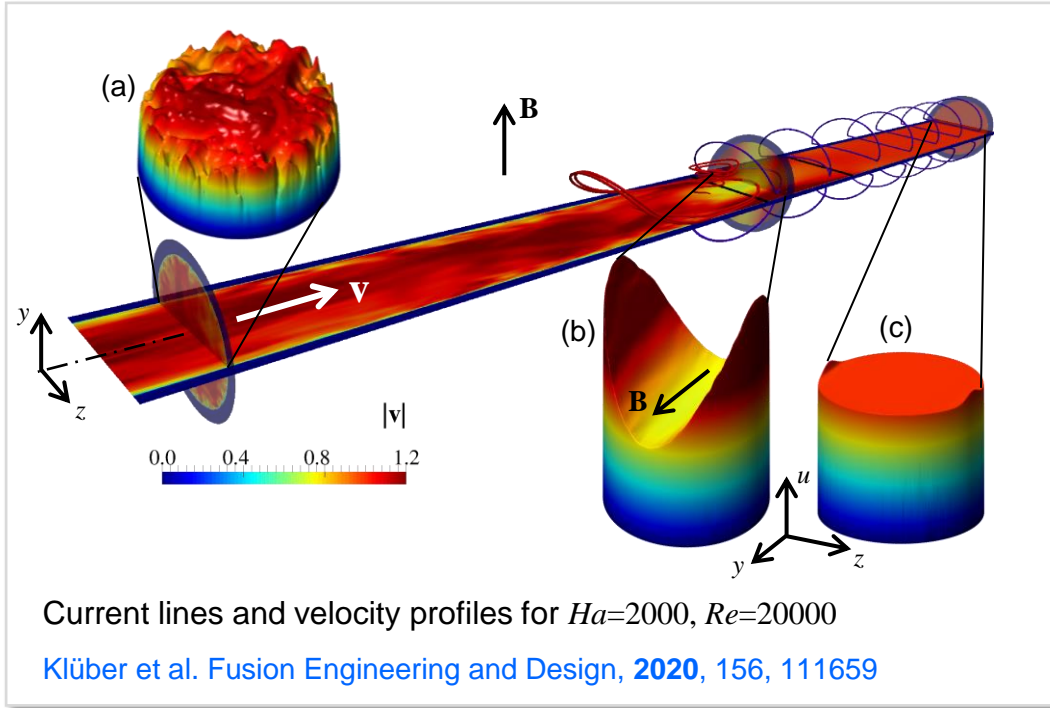
- ❑ high velocity at sides
- ❑ reduced velocity in center



$$u(y, z) \approx B^{-1} \frac{\partial \phi}{\partial z}$$

Flow in non-uniform B-field

Numerical simulation of turbulent flow entering a magnetic field



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Magneto convective heat transfer at cooling pipes

Experimental and theoretical results are available for

- Rayleigh – Bénard convection (differentially heated horizontal layer of fluid)
- differentially heated vertical gap
- heat transfer in pipe and duct flow

Zikanov et al. Mixed convection in pipe and duct flows with strong magnetic fields, *Applied Mechanics Reviews*, **2021**, 73, 010801-1-35

Lack of knowledge on

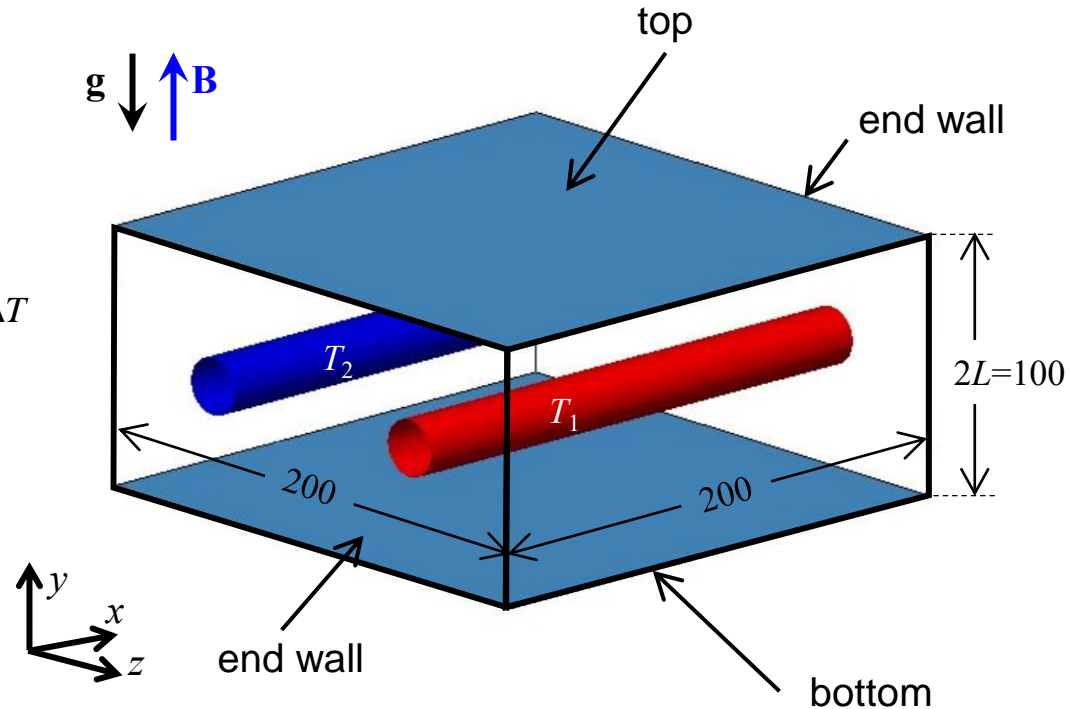
- MHD flows around obstacles with heat transfer (cooling pipes)
 - need for analyses → definition of a generic problem

Magneto-convection around obstacles

Definition of generic problem

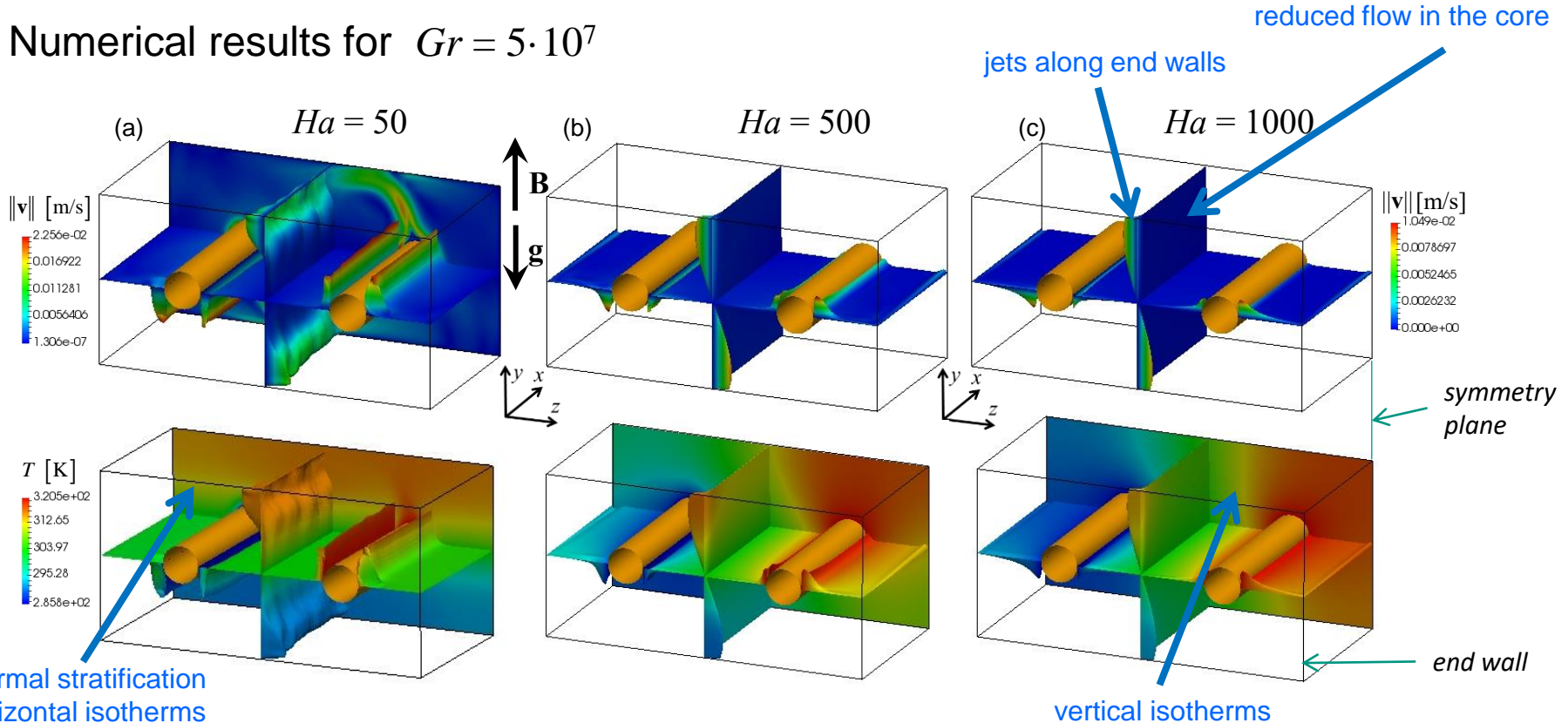
- ❑ adiabatic box filled with GaInSn
- ❑ electrically insulating walls
- ❑ differentially heated cylinders $T_{1,2} = \bar{T} \pm \Delta T$
- ❑ Parameters:

$$Gr = \frac{g\beta\Delta TL^3}{\nu^2}, Ha = BL\sqrt{\frac{\sigma}{\rho\nu}}$$



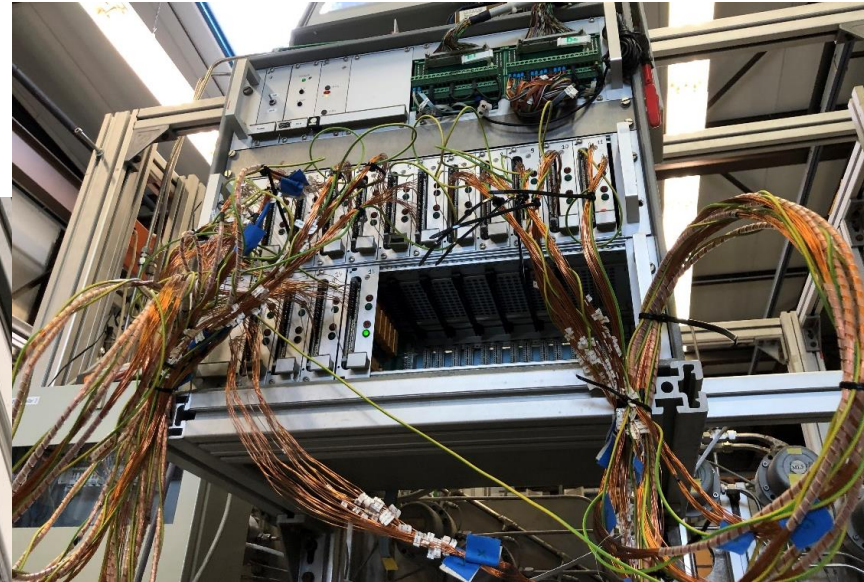
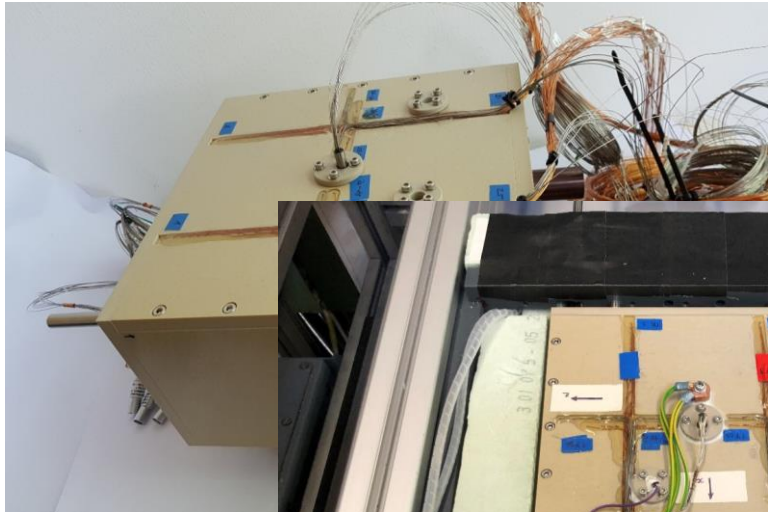
Magneto-convection around obstacles

Numerical results for $Gr = 5 \cdot 10^7$



Magneto-convection around obstacles

Experiments



Magneto-convection around obstacles

thermal stratification
horizontal isotherms

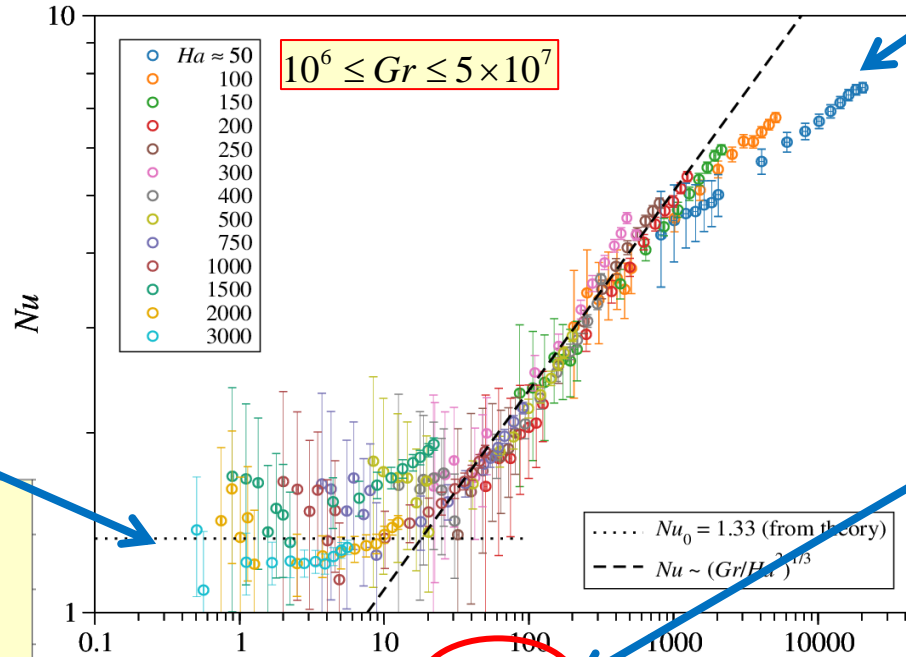
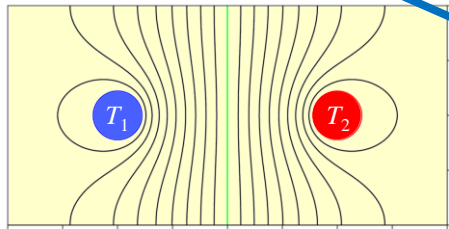
Heat transfer quantified by Nusselt number

$$q'' = h \Delta T$$

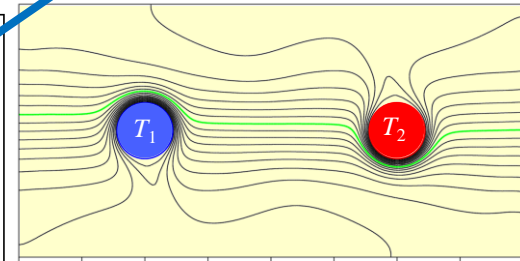
$$Nu = \frac{hL}{k}$$

vertical isotherms
heat conduction

-- no flow --



-- strong convection --



results depend on
combination of Gr and Ha

$$\frac{Gr}{Ha^2} = \frac{\text{buoyancy force}}{\text{electromagnetic force}}$$

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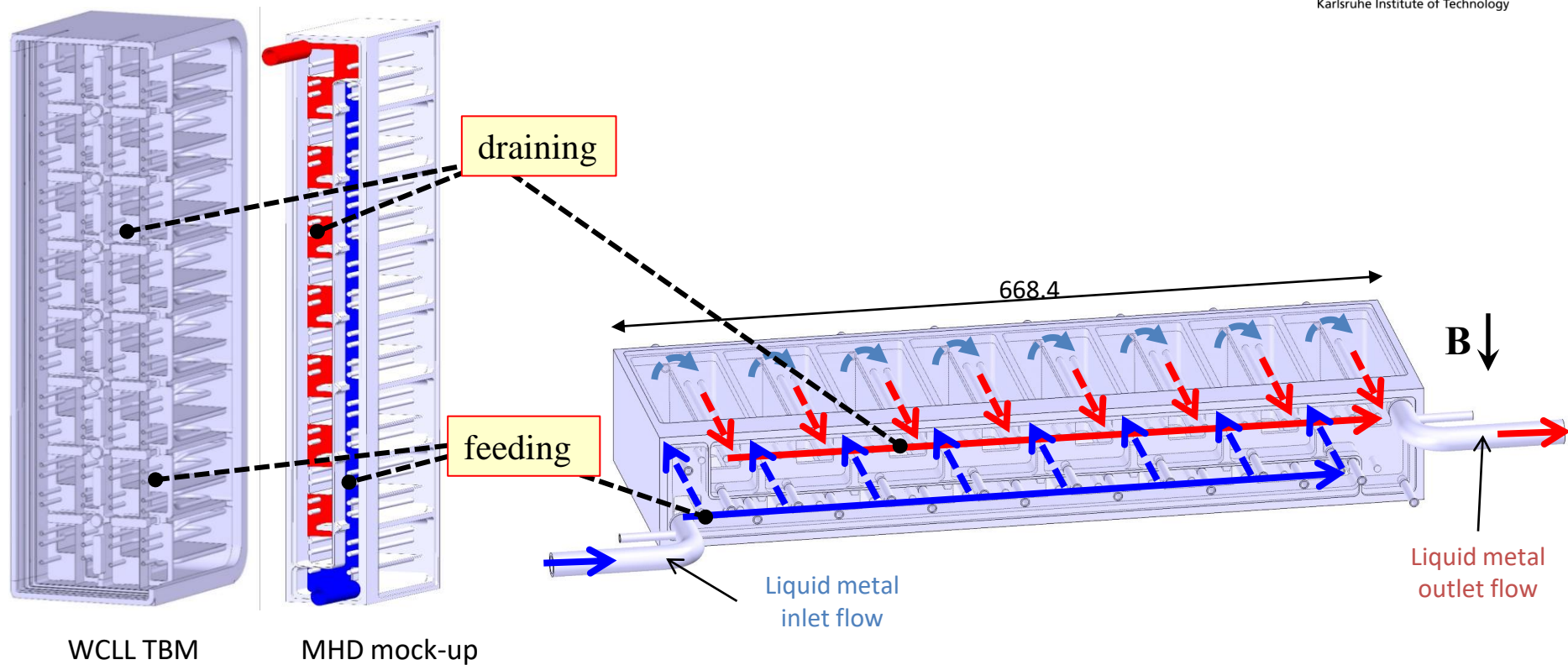
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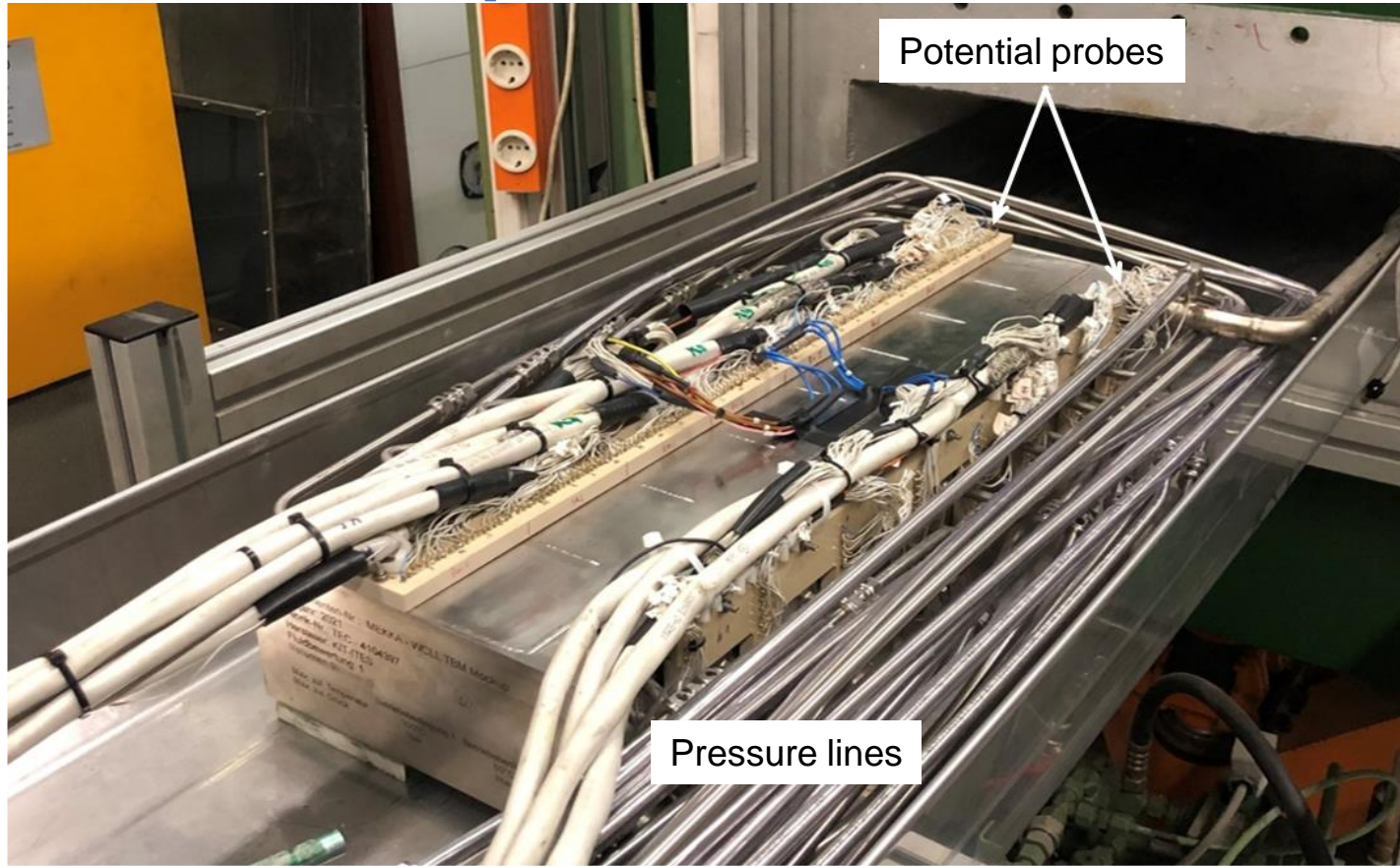
Flow in a complex WCLL TBM-like geometry

TBM mock-up in MEKKA

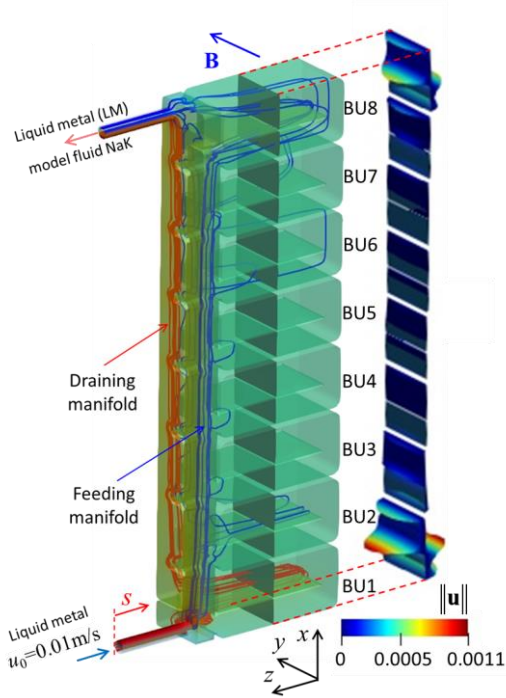


Koehly et al. *Fusion Engineering and Design*, 2023, 192, 113753

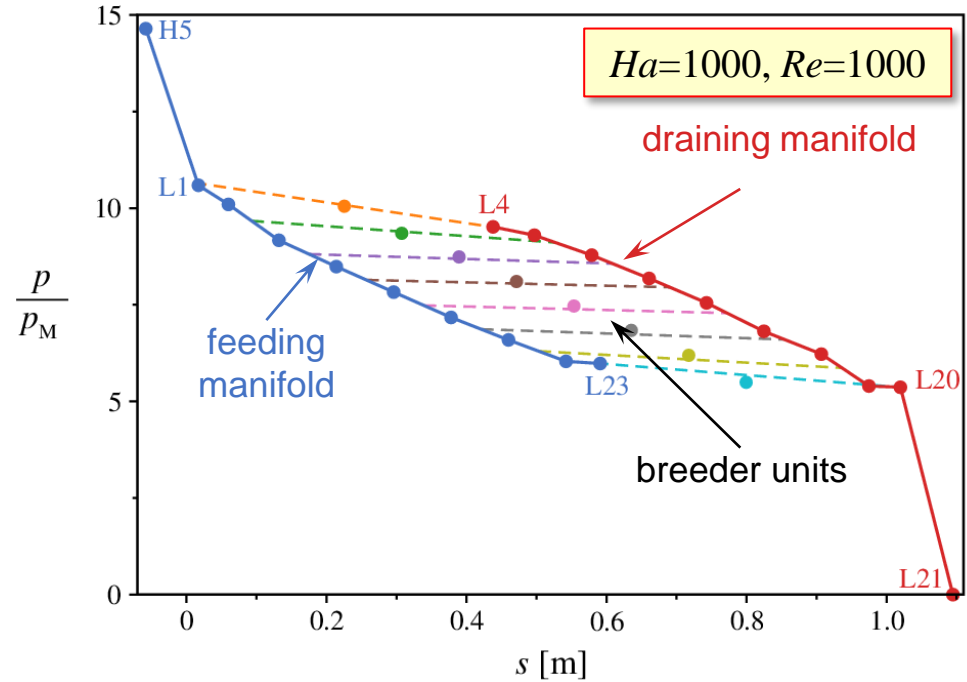
TBM mock-up in MEKKA



Experiments in MEKKA and simulations

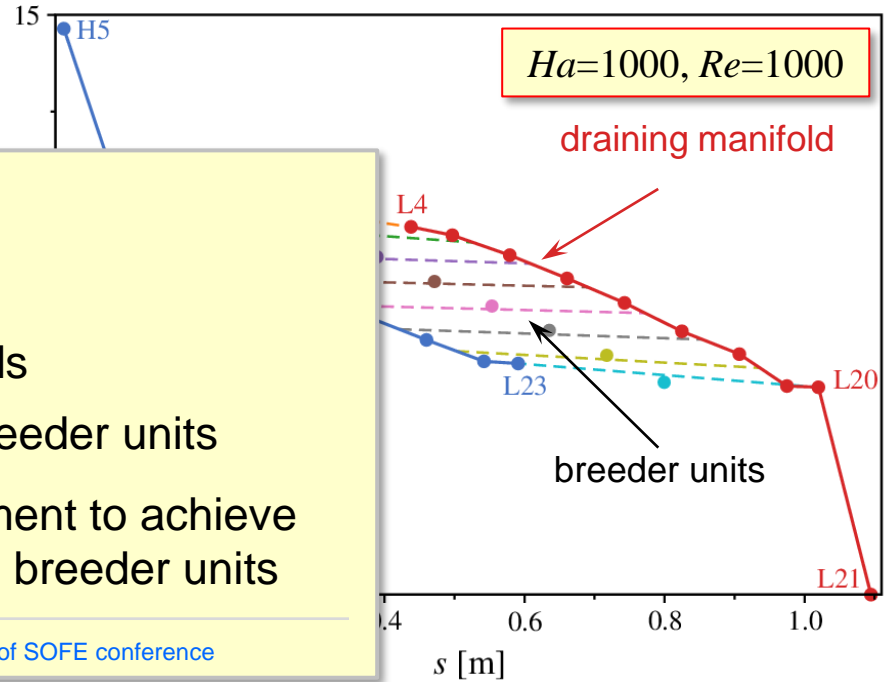
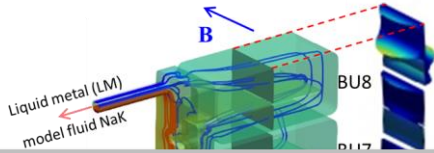


Numerical simulation: Flow paths along manifolds and BUs and radial velocity profiles in middle plane



Measured pressure distribution along typical flow paths

Experiments in MEKKA and simulations



Results

- total pressure drop is acceptable
- major pressure drop occurs in manifolds
- non-uniform flow distribution among breeder units
- suggestions made for design improvement to achieve more homogeneous flow partitioning in breeder units

Bühler & Mistrangelo, 2023 *IEEE Transactions on Plasma Science*, Proc. of SOFE conference

Numerical simulation: Flow paths along manifolds and BUs and radial velocity profiles in middle plane

Measured pressure distribution along typical flow paths

Summary and future plans

MHD research at Karlsruhe Institute of Technology KIT

- ❑ MEKKA and MaPLE
- ❑ Development of predictive tools
- ❑ Study of MHD flows for fusion relevant parameters
 - ❑ basic research
 - ❑ applied engineering problems

Outlook

- ❑ Full commissioning of MaPLE
 - ❑ first experiments in a circular pipe → pressure drop → potential data, → $\mathbf{B}(x)$
 - ❑ mixed convection MHD heat transfer → horizontal, inclined, vertical ducts
- ❑ Scaled blanket mock-up test in MEKKA magnet with PbLi from MaPLE

Results will support theoretical developments and blanket engineering



EUROfusion



This work has been carried out within the framework of the EUROfusion Consortium, funded by the European Union via the Euratom Research and Training Programme (Grant Agreement No 101052200 — EUROfusion). Views and opinions expressed are however those of the author(s) only and do not necessarily reflect those of the European Union or the European Commission. Neither the European Union nor the European Commission can be held responsible for them.

