



Effect of Recrystallization on Fatigue Crack Growth Characteristics of a Pure Tungsten

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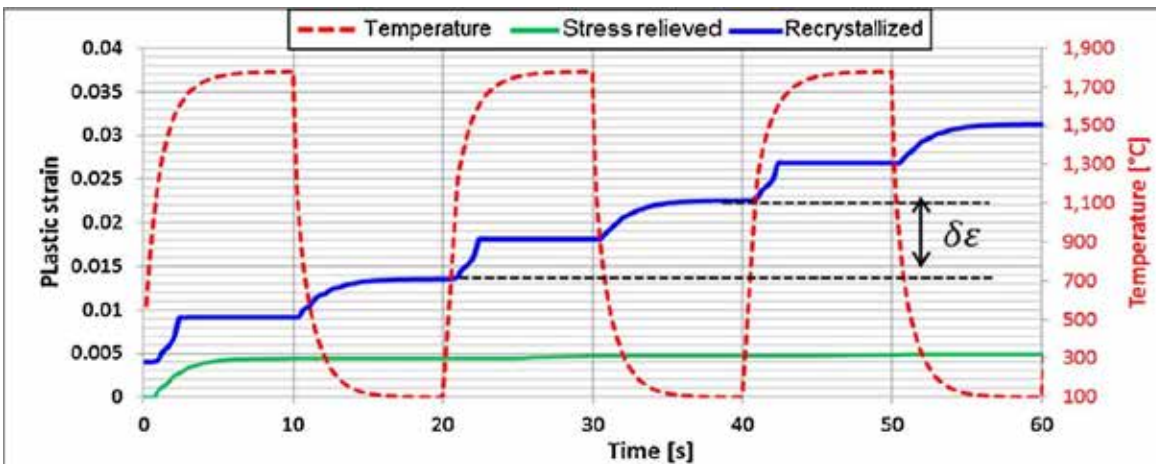
✓ Plasma facing material (PFM) in fusion reactors

∅ Characteristics of tungsten considered as PFM

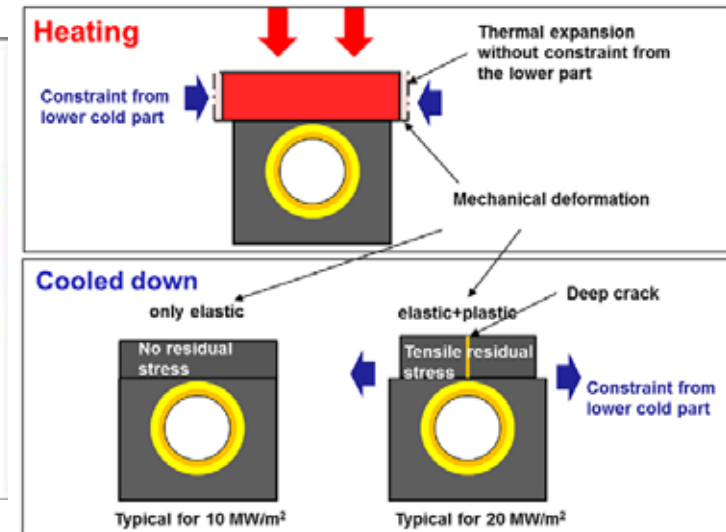
- High melting point, high thermal conductivity, and low tritium retention [1]
- Inherent low fracture toughness, high DBTT and low Recrystallization temperature

∅ Thermal fatigue of PFM armor under high-heat flux (HHF)

- Tungsten(W) exposed to HHF in-service reactor [2]
- PFM exhibits high temperature gradient due to HHF cycles and coolant pipe **Thermal fatigue**
- Fatigue crack generated by thermal fatigue [3]



A schematic representing the temperature history of tungsten armor under HHF cycles [2]



A schematic of the deep crack mechanism of tungsten armor under HHF cycles [3]

✓ Plasma facing material (PFM) in fusion reactors

∅ Recrystallization effect of heat flux facing surface of PFM

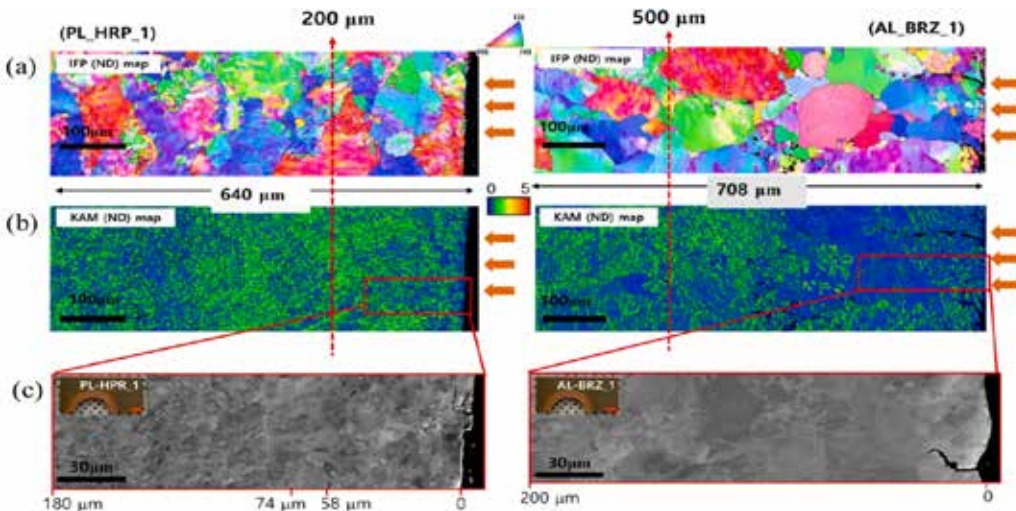
- H.C. Kim et al., Fusion Eng. Des. 170 (2021) 112530

- Apply HHF test at 10 MW/m² up to 5,000 cycles, recrystallization phenomena is observed [4]
- Decreasing yield strength due to recrystallization may promote fatigue crack [5]

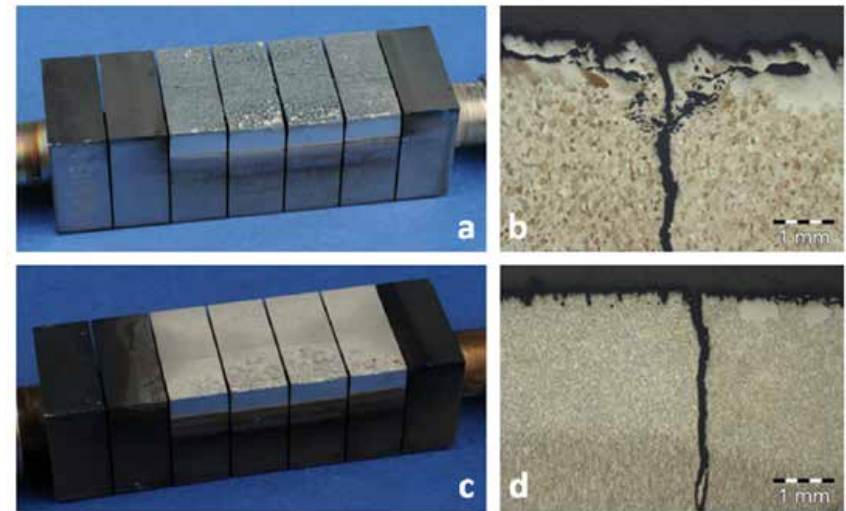
- G. Pintsuk et al., Fusion Eng. Des. 98-99 (2015) 1384-1388

- Apply HHF test at 20 MW/m² up to 1,000 cycles, macro-crack is observed [4]
- Deep cracks propagate in brittle mode to the W/Cu interface

Evaluation of fatigue crack growth on tungsten is crucial



Microstructure profile of the HHF tested plansee and ALMT W in the surface region [4]



Macro-crack image created on tungsten mock-up and surface exposed to HHF [6]

Evaluation of Recrystallization Effect on Fatigue Crack Growth Characteristics of a Pure Tungsten

Evaluation of J-integral Property considering strain-rate and Rx



EBSD analyses for investigating evolution of microstructure

∅ Evaluation of **High Temperature Mechanical Properties** of Pure Tungsten for Integrity of ITER Divertor

✓ Test Material : A.L.M.T Tungsten (W)

∅ IQ + IPF map

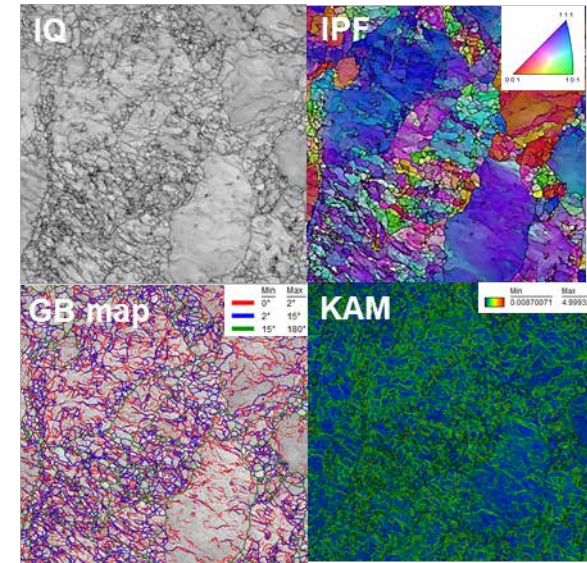
- Sub-grain structure within large grains (TMP)

∅ Grain Misorientation map

- LAGB Fraction (~ 80%)
- HAGB Fraction (~ 20%)

∅ KAM map

- Deformation energy is homogeneously distributed



The EBSD results of A.L.M.T tungsten; (a) IQ, (b) IPF, (c) GB maps, and (d) KAM

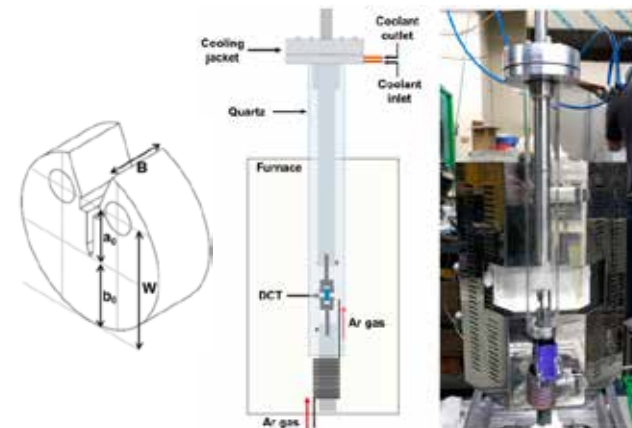
✓ Test Specimen & Facility

∅ Smaller disc compact (DCT) specimen

- Specimen geometry : $a_0 = 2.7$ mm, $b_0 = 3.3$ mm, $B = 1.5$ mm
 - Complied with general proportions of ASTM-E399 & E1820
- Notch direction perpendicular to the longitudinal direction
- **Notch root radius of the machined notch : ~ 70 μ m**

∅ Test facility set-up in Ar environment

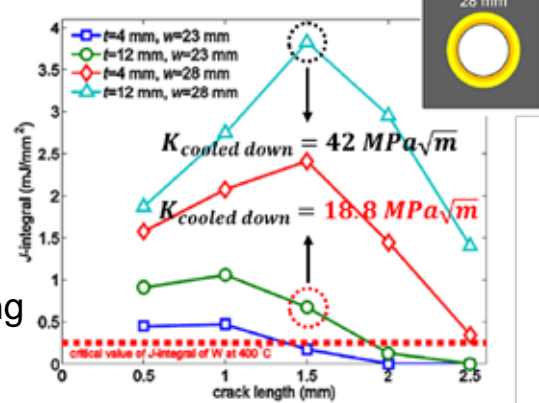
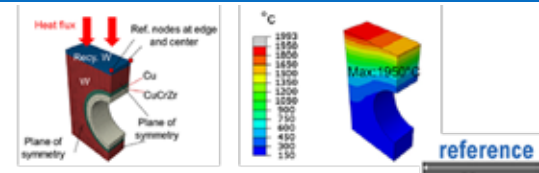
- To prevent excessive oxidation in high temperature
 - **Ar gas was injected into the quartz (Flow rate: 2K cc / min.)**



The Schematics of specimen and facility [1] Nuclear & High Temperature Materials Lab.

✓ Fatigue Crack Growth Rate Test Procedure

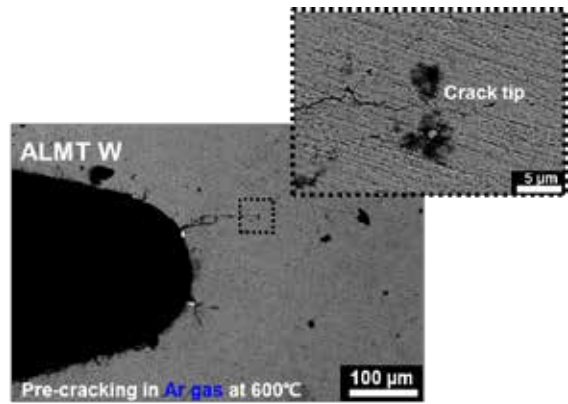
- ∅ Refer to simulation data assuming crack [2,3]
 - $\Delta K = K_{max} - K_{min} = \sim 20 \text{ MPa}\sqrt{\text{m}}$, $R = 0.1$, ($\dot{\epsilon} = 3.0 \times 10^{-2} \text{ s}^{-1}$)
 - Perform K -increasing FCGR test ($P_{max} = 250 \text{ N}$)
- ∅ Fatigue pre-crack process at elevated temperature
 - Considering inherent brittleness (At higher than DBTT)
 - Introducing pre-crack in Ar environment through tensile cyclic loading
 - Sharp pre-crack without oxides (Notch root radius $\sim 0.2 \mu\text{m}$)



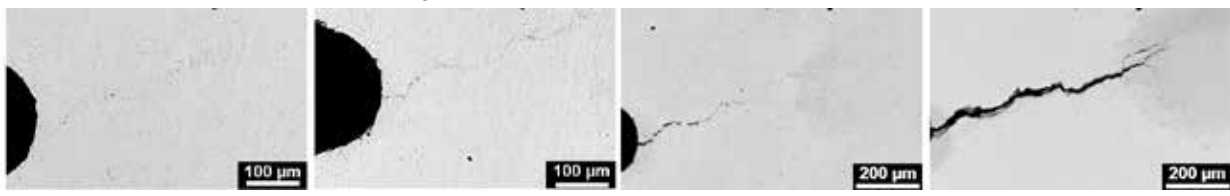
J-integral values at the tip of a crack initiated at the armor surface [2,3]

∅ Calculating the da/dN and ΔK values

- Measuring crack length using SEM (Difficulty using DCPD and COD)
- Plot the graph after calculating the da/dN and $\Delta k_{Aver.}$ using parameters



The morphology of fatigue pre-cracks



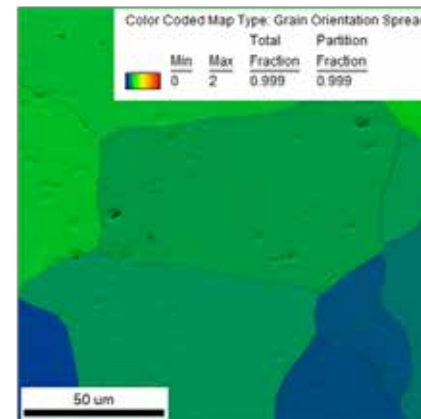
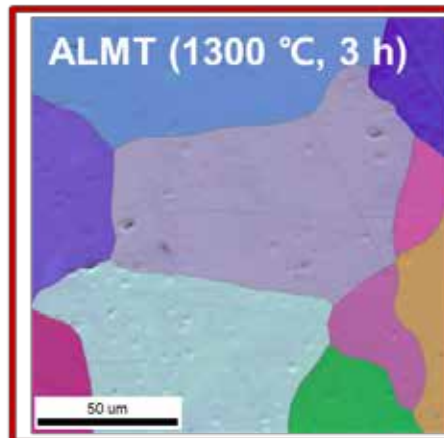
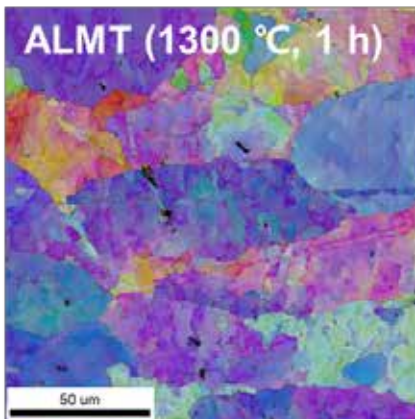
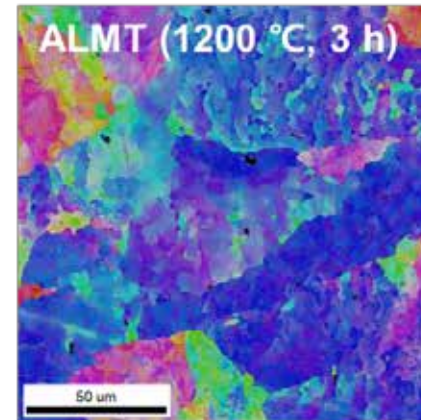
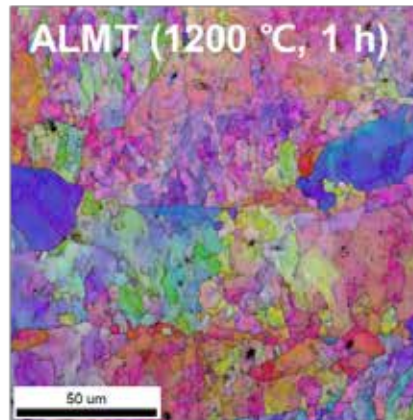
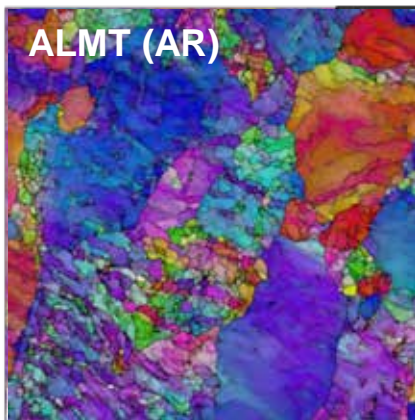
crack length (mm)	Crack length + notch	$\alpha = a/W (>0.2 \text{ valid})$	Geometry constant	da/dN [m]	da/dN [mm]	del K (Average)
0.21	2.91	0.49	9.71	6E-06	6E-09	18.81
0.24	2.94	0.49	9.86	3.1E-05	3.1E-08	19.09
0.33	3.03	0.51	10.36	9.3E-05	9.3E-08	20.07
0.45	3.15	0.53	11.07	1.2E-04	1.2E-07	21.44
0.62	3.32	0.55	12.18	1.7E-04	1.7E-07	23.58
0.89	3.59	0.60	14.42	2.7E-04	2.72E-07	27.92

Procedure of calculating the da/dN and $\Delta K_{Aver.}$

Results – Recrystallization condition

✓ Recrystallization condition of ALMT W

- ∅ Heat treatment trials for finding recrystallization condition
- ∅ EBSD results of ALMT W (1300 °C, 3 h)
 - Grain Orientation Spread ($0^{\circ}\sim 2^{\circ}$) : Fully recrystallized W



Procedure of calculating the da/dN and ΔK

Results – Tensile results

✓ Tensile test results of pure tungsten

∅ Tensile results of As-Received W

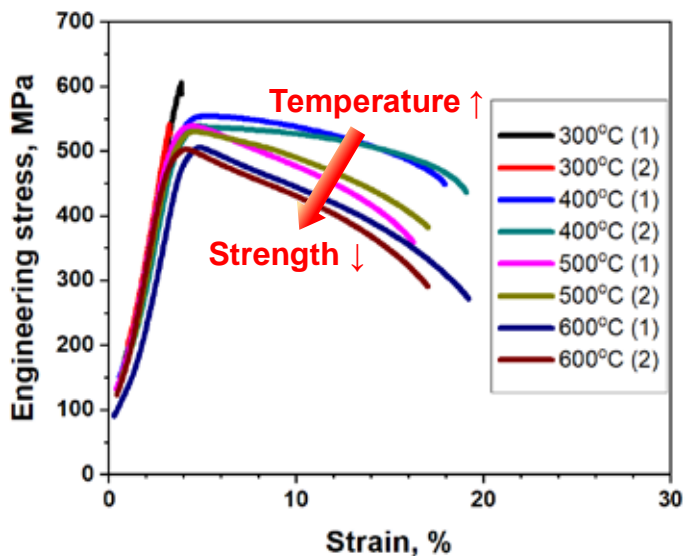
- Strength is decreased with increasing temperature
- Brittle behavior is observed below 300

∅ Tensile results of Recrystallized W

- As temperature is increased, strength is decreased and elongation is significantly increased
- Brittle behavior is observed below 500

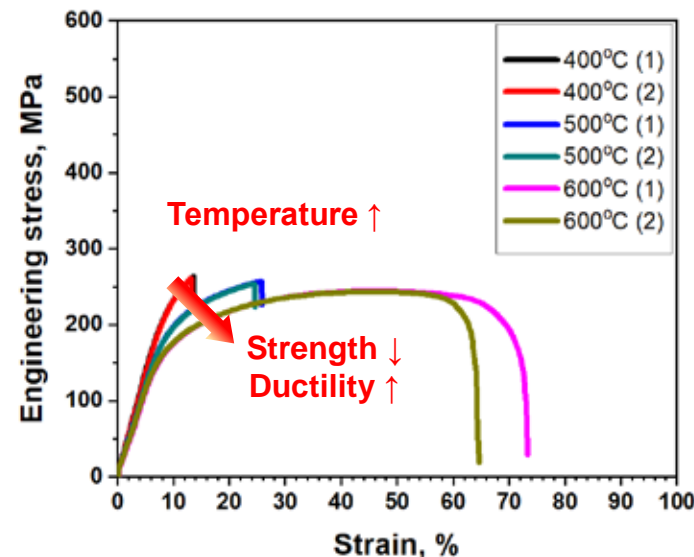
Using tensile results for evaluation of J-integral property and FCGR characteristics

<ALMT W>



Recrystallization

<RXed ALMT W>



Results – FCGR characteristics

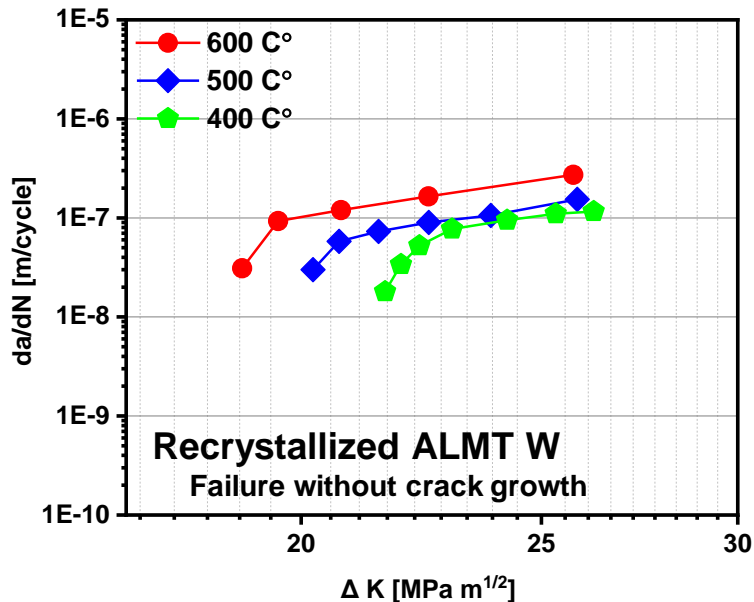
✓ FCGR Test results

∅ Plot the da/dN-ΔK curve using measuring crack length

- FCGR tests are conducted at elevated temperatures
 - At 400 – 600
 - As temperature is increased, FCGR characteristic is decreased
 - All Recrystallized ALMT W is brittly fractured

∅ Calculating the parameters of Paris's law

- These constants were determined by curve fitting



$$\text{Paris's Law : } \frac{da}{dN} = C \cdot \Delta K^m$$

Condition	Temperature	C	m
As-Received ALMT	600	1.25×10^{-12}	3.78
	500	7.71×10^{-12}	3.01
	400	3.98×10^{-11}	2.42
RXed ALMT	600	-	-
	500	-	-

da/dN-ΔK graph of ALMT W

Procedure of calculating the da/dN and ΔK

Results – FCGR characteristics

✓ Fractography of FCGRed Test specimen

∅ As-Received ALMT W

- Fatigue crack growth regions were observed
- Calculate K_{max} value using Fatigue crack growth region of As-Received ALMT W

∅ Recrystallized ALMT W

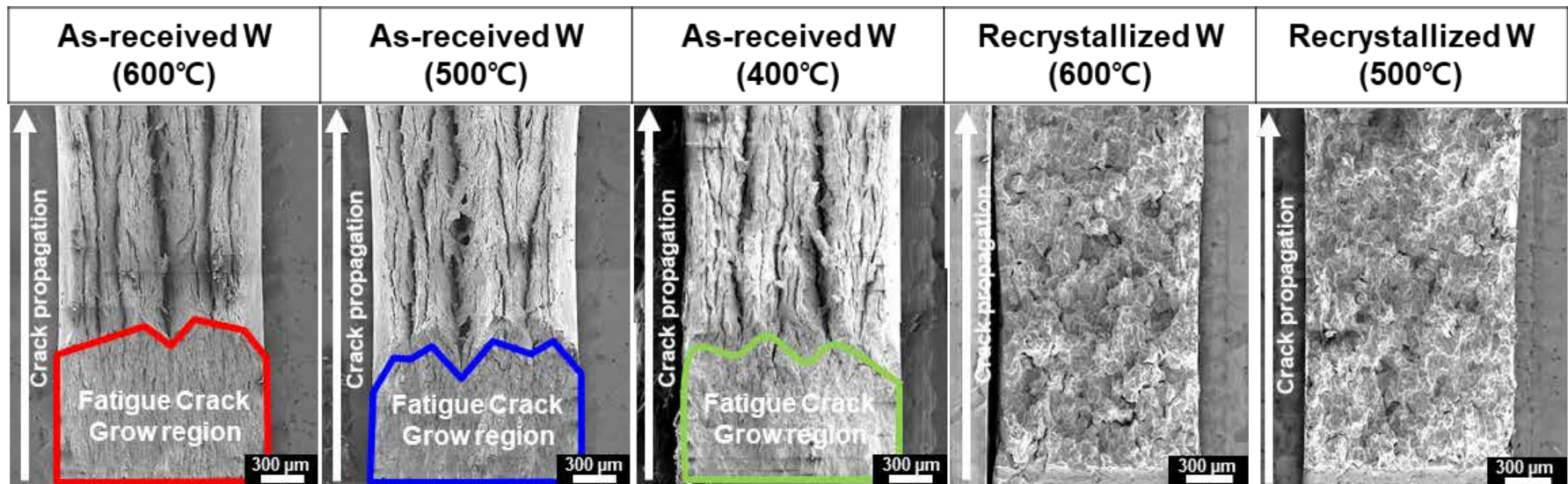
- Intergranular failure without fatigue crack growth

<Estimated value>

* $K_{max., 600^{\circ}\text{C}} = 29.5 \text{ MPa}\cdot\text{m}^{1/2}$

* $K_{max., 500^{\circ}\text{C}} = 28.6 \text{ MPa}\cdot\text{m}^{1/2}$

* $K_{max., 400^{\circ}\text{C}} = 27.3 \text{ MPa}\cdot\text{m}^{1/2}$



SEM fractography of as-received and recrystallized ALMT W

Results – Effect of Strain-rate in J-integral property

Effect of Strain-rate in J-integral property

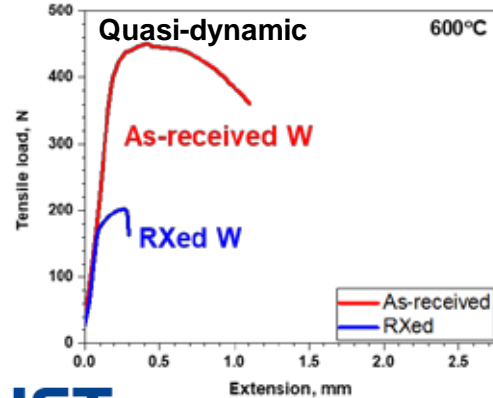
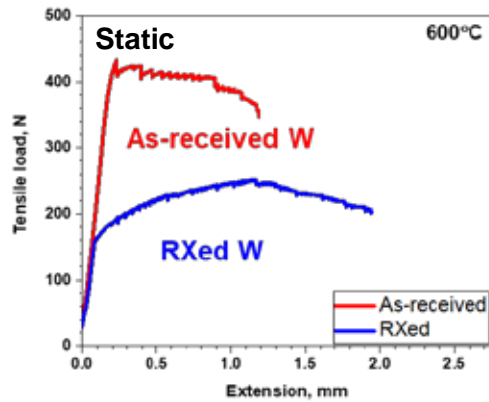
Static condition ($1.33 \times 10^{-4} \text{ s}^{-1}$)

- Similar J-integral properties

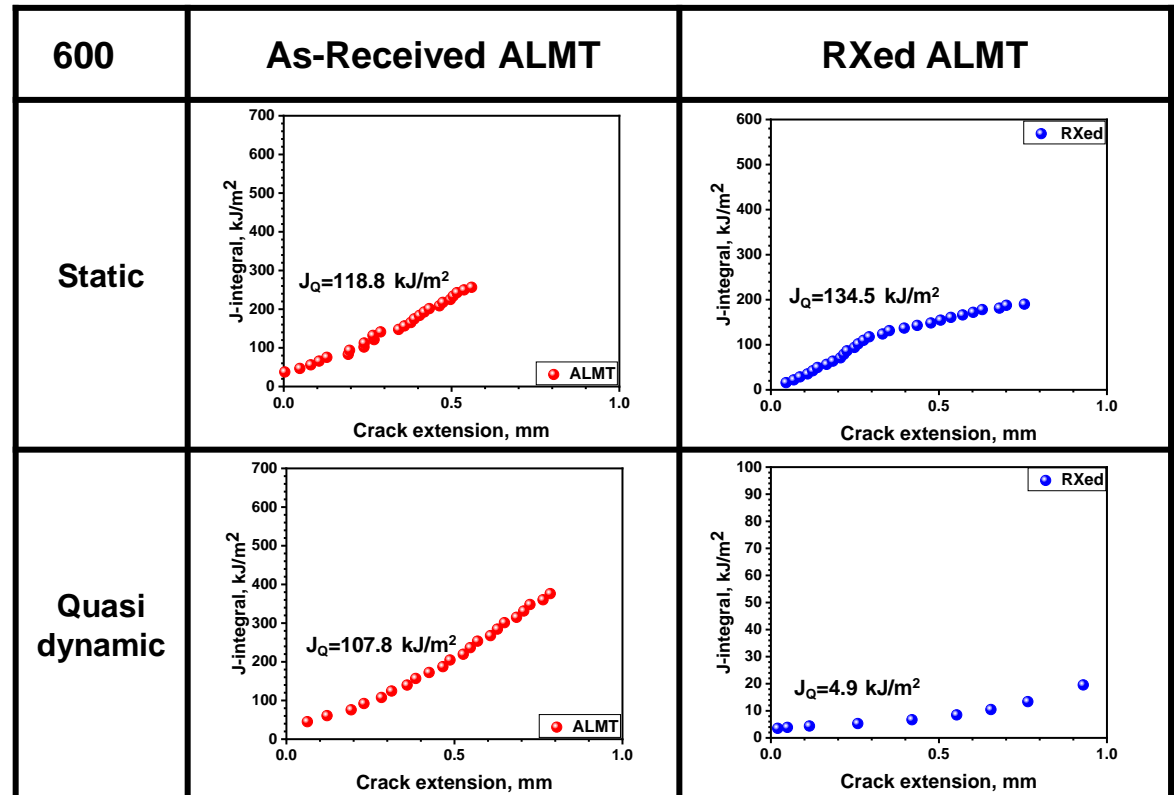
Quasi-dynamic condition ($5.30 \times 10^{-2} \text{ s}^{-1}$)

- J-integral property of Recrystallized W is significantly decreased

Load-Extension curve at 600



J-integral curve at 600



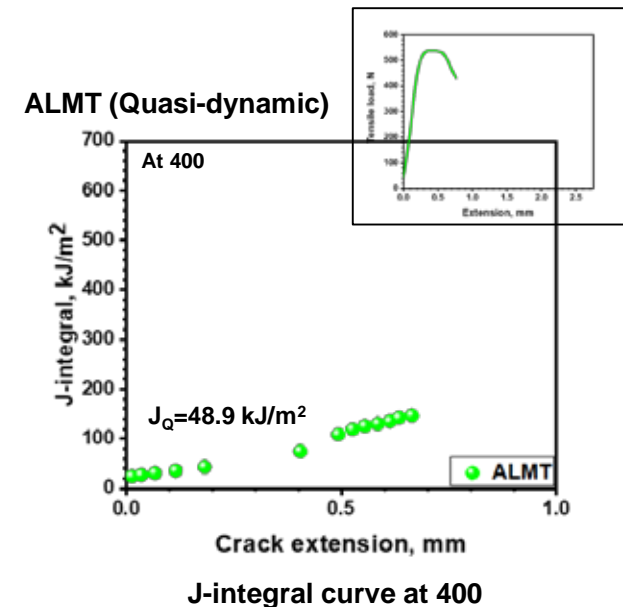
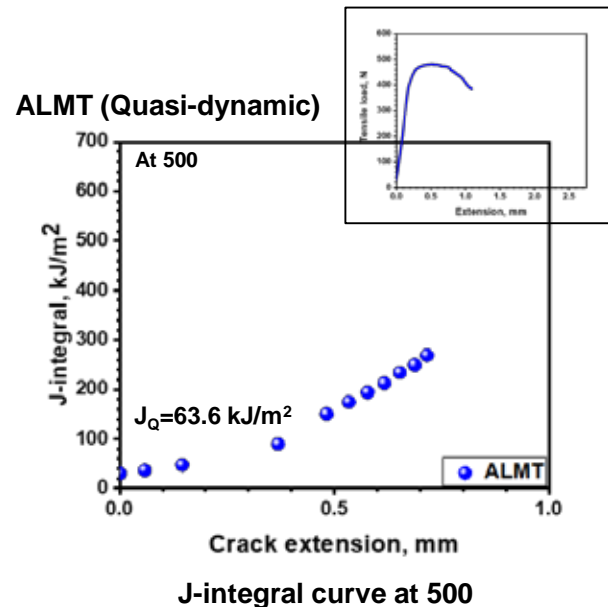
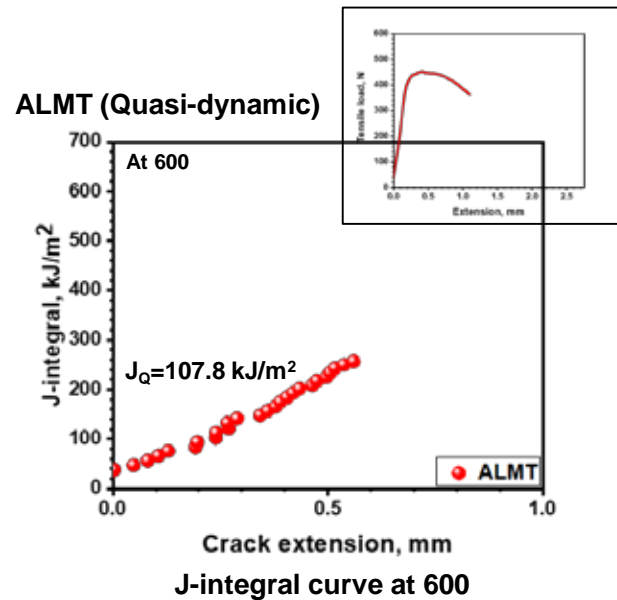
Results – Effect of Temperature in J-integral property

✓ Effect of Temperature in J-integral property (High strain rate)

∅ High strain rate condition ($5.30 \times 10^{-2} \text{ s}^{-1}$)

- 600
 - $J_Q=107.8 \text{ kJ/m}^2$
- 500
 - $J_Q=63.6 \text{ kJ/m}^2$
- 400
 - $J_Q=48.9 \text{ kJ/m}^2$

As temperature is decreased, J-integral property is decreased



Results – Effect of Temperature FCGR characteristics

Effect of Temperature in FCGR characteristics

Considering the starting point of regime B

Referring the $da/dN - \Delta K$ graph

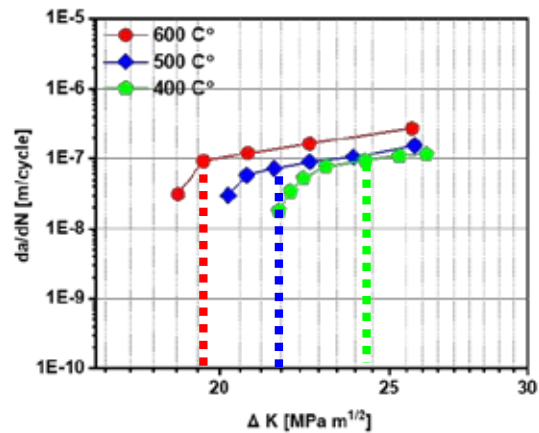
600 (~ 334 μm), 500 (~ 494 μm), and 400 (~ 710 μm)

EBSD results of FCGRed specimens

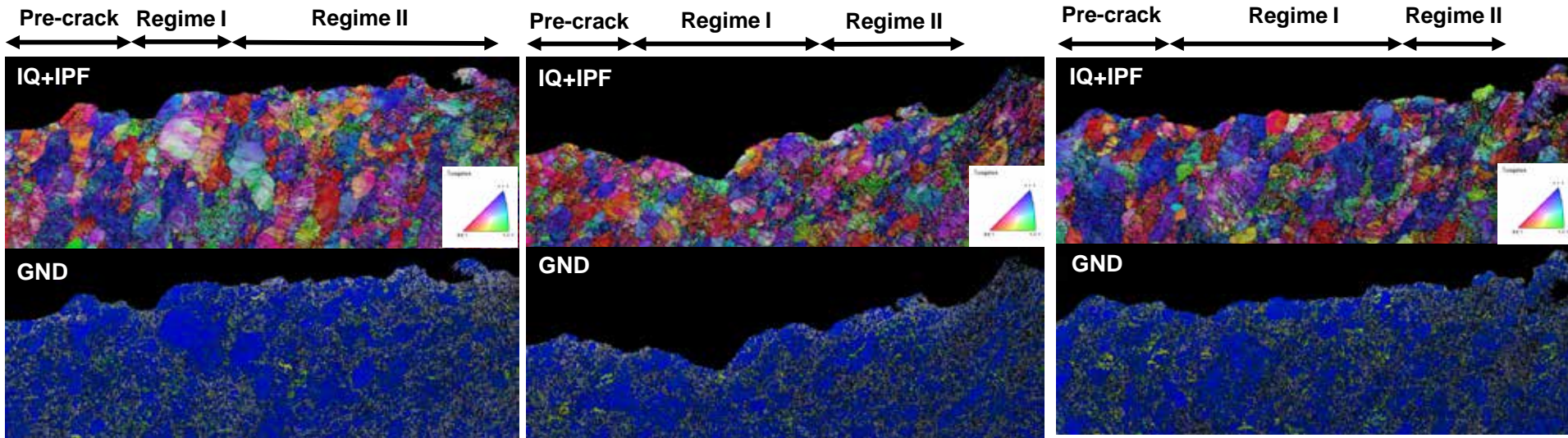
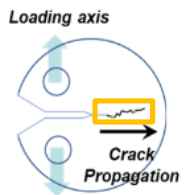
- Compared to graph, starting points of regime B are similar
- Dynamic recrystallization is observed through EBSD result**

As temperature is increased, DRX is increased

As temperature is decreased, starting point of regime B moves away



da/dN-ΔK graph of ALMT W



EBSD results of FCGR test at 600

EBSD results of FCGR test at 500

EBSD results of FCGR test at 400



Energy for Earth !!



Thank you!

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