

ISFNT-15

The Lead Lithium Loop for the European Water-Cooled Test Blanket System (WCLL-TBS)

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14th September 2023

Special thanks to I. Ricapito, A. Aiello & A. Tincani







- **1.- Brief Introduction to the Test Blanket Systems**
- 2.- Specificities of the Water-Cooled Lithium Lead (WCLL) TBS
- 3.- The Lead-Lithium (PbLi) Loop for the ITER TBS
- 4.- Main Challenges and Achievements of the PbLi loop in ITER
- **5.- Open Issues & Conclusions**



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2.- Specificities of the Water-Cooled Lithium Lead (WCLL) TBS





The coolant is pressurized water at 15.5 MPa, 295 - 328 °C and 3.74 kg/s

The breeder is molten Pb16Li that is circulated to promote external (to the TBM) tritium extraction. PbLi is circulated by <u>the PbLi loop</u> at 0.16 MPa, 295 - 322 °C and 0.65 kg/s

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- To provide, circulate and maintain PbLi eutectic alloy at operating conditions suitable for the WCLL-TBM correct operation
- To move tritium from TBM to promote external tritium extraction
- To remove impurities from the PbLi alloy
- To provide confinement for PbLi, helium and radioactive products
- To ensure the implementation of the safety functions











- High component density due to lack of space
- Maintenance not easy when AEU in port
- Layout to be reviewed for integration purposes with new AEU volume



Magnets

Main Components: Function and Technology

Pump

- Permanent magnets pump;
- Advantage to avoid contact between moving parts and PbLi;
- Components subject to maintenance are external to the PbLi flow;
- Residual volume in the loop during operation is strongly reduced.







Tritium Extraction Unit (TEU)

- Gas-Liquid Contactor in packed columns configuration
- More stable & Mature than other concepts (i.e. PAV)
- Extraction performance (\approx 40 %) is stable along time but depends on flow parameters
- Low maintenance unit

Cold Trap (CT)

- **Finned cylindrical steel labyrinth**
- No moving parts inside but subject to the formation of plugs due to low temperature (265 °C)
- The external fan increasing the air-flow through the fins is a concern with regards reliability
- The maintenance (i.e. replacement) of this unit is very complex



Cold Trap





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This Section is divided in three main blocks:

- 1.- Dose rate in PC #16 exceeding limits (PbLi as main contributor)
- 2.- Integration in ITER and space constraints
- 3.- Specific Research & Development needs

For these three points the next slides will present the challenges / issues, the achievement and the next steps





Dose rate in PC #16

Cat. I Chit at CDR

	Total biological dose rate after 1 day in PC (μ Sv/h)							
AEU-PC tally	Activated Components	PbLi layer in pipes	PbLi in storage tank and cold trap	АСР	Total			
1 - PC entrance door	0.1	21.0	0.2	0.0	21.3			
2 – Lateral stairs	0.9	555.6	1.9	0.2	558.5			
3 – AEU platform Pos1	0.2	77.5	0.7	0.1	78.5			
4 – AEU platform Pos2	0.4	306.7	1.6	0.4	309.0			
5 – AEU platform Pos3	0.7	1419.2	6.4	0.4	1 426.8			
6 – AEU platform Pos4	1.2	3197.1	1.5	0.5	3 200.4			
7 – AEU platform Pos5	1.1	1305.9	0.4	0.5	1 307.9			
8 – Back BP right side	5.2	1864.0	1.1	0.6	1 870.9			
9 – Back BP left side	4.6	1481.0	1.6	1.0	1 488.3			
10–Cold trap	0.1	454.5	264.4	0.4	719.4			
11 – Flow meter	0.9	5441.6	11.5	0.1	5 454.2			
12 – Valves	1.2	2693.0	0.5	1.8	2 696.5			
13 – PbLi pump	0.1	1191.2	0.4	1.5	1193.2			
14 – Back Valves	0.3	50.3	0.5	0.4	51.8			
15 – Vacuum pump in PC	0.3	238.1	13.8	0.6	252.9			

Dose rate limit after 24 h: 10 µSv/h

Without taking into account the PbLi residual layer contribution, the limit of 10 μ Sv/h is met almost in all tallies

Challenges 1/2

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Dose rate in PC #16 Challenges 2/2

Cat. I Chit at CDR

Dose rate limit after 24 h: 10 µSv/h

Total biological dose rate source contribution maps @ 1 day



Dose rate in AEU side of the PC is mainly due to residual PbLi layer inside the pipes.



Dose rate in PC #16 Achievements

The main reason for exceeding dose rate limit was the assumed layer of activated PbLi that remained inside the loop after drainage. The 1 mm thickness of PbLi layer considered during the CDR resulted to be an over-conservative assumption.

- Examining the data from experimental PbLi loops operated in Europe, thicknesses for the residual layer of about 50 μm have been found. This has been confirmed by parametric CFD analysis providing results in the same range (as low as ≈10 μm).
- to achieve this residual layer thickness the PbLi loop shall:
 - i. implement a slope of at least 3 %;
 - ii. maintain a temperature of at least 295°C during drainage;
 - iii. be drained during at least 24 hours;
- in addition, local nuclear shielding shall be put in place. Preliminary values for the shielding are 10 mm of lead or 55 mm of steel);
- A preliminary check on the 3D model has confirmed the feasibility to implement the changes having an impact on the PbLi loop layout (i.e. slope and shielding);

With all the above changes implemented, the resulting dose rate is lower than the limit of 10 µSv/h

Dose rate in PC #16 Next Steps



- A PbLi residual layer of 100 µm has been assumed to be a conservative but realistic value. This
 means that use of lead shielding instead of steel provides significant improvement in terms of
 used space. At the same time the lead shielding shall be encapsulated to avoid issues due to
 lead low melting temperature. The piping layout has been defined as follows and needs to be
 fully implemented;
- The value of the pipe slope has been conservatively set as 5% with a minimum of 3% in some areas if needed. The new thickness of shielding and the pipe slope have been preliminary implemented in a 3D model but it needs to be finalized and improved:
- A new nuclear analysis is being developed so:
 - i. the results in terms of dose rate reduction can be confirmed within the limits;
 - ii. a parametric analysis is performed to improve shielding thicknesses;
 - iii. the precise new layout of the PbLi loop is taken into account (i.e. slope);





Image courtesy of NIER Ingegneria







Integration in ITER Challenges

- > Integration has many different aspects that shall be taken into account:
 - We are going to install a Test Blanket System in an INB ("Instalation Nucleaire de Base") -> Regulations
 - ITER is not a dedicated facility -> TBSs co-exist with many other systems
 - TBSs are not essential for the operation of the machine -> need to accommodate last minute changes
 - TBSs are experimental devices -> unique and complex sub-systems (i.e. PbLi loop is unique in ITER)
 - Different design responsibles for different parts of the sub-systems
- These particularities make needed to:
 - Deploy the different sub-systems among different locations in the tokamak complex -> 3 different rooms
 - Have interfaces with many other PBS (e.g. services) -> WCLL-TBS interfaces with up to 27 different PBSs
 - Accommodate the systems into the available space









In order to synchronize the different stakeholders and to solve the integration issues in PC for PDR:

- > First action on simplifying the systems as much as possible
 - Three stakeholders have been requested to **simplify and remove** components -> gain space
 - The main idea behind is to **ensure feasibility** of having two TBSs in one port
- Second action to create a Work-Plan up to PDR for integrated activities
 - It is clear that some activities require an integrated analysis (e.g. heat release)
 - These analyses shall be executed by one of the three entities but feed by the other two
 - Since PDR is approaching fast a detailed work-plan is needed so the three parties can organize their resources



Research & Development Ongoing Tasks

- Sas-Liquid Contactor (TEU) characterization for WCLL-TBS: first set of experiments and data analysis;
- > Tritium Sensors in PbLi (permeation and potentiometric sensors);
- > Selection and qualification of Thermal-Hydraulic sensors in PbLi (pressure, mass flow rate, level);
- > Coupling of Relap5 and Simmer to perform analysis at system level;
- Development of the DEMO PbLi code for the TBM Project
- > Execution of tests on WCLL-TBM PMU in IELLLO and data elaboration

R&D Activities developed in partnership with





Research & Development Some Details 1/2

Development of the DEMO PbLi code for the TBM Project

- It is expected to have in the end a unique code capable to simulate the lead lithium loop, from a TH point of view, in normal and accidental conditions, coupling the different involved phenomena.
- Integration in Relap5 of:
 - updated PbLi fluid libraries
 - the phenomena of transport for non-mixable species
 - Magneto-Hydro-Dynamic (MHD) effects

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Research & Development Some Details 2/2

- Execution of tests in IELLLO (Integrated European Lead Lithium LOop) and data elaboration to feed the design with:
 - the real thickness of residual PbLi in pipes after drainage;
 - the maximum length of pipe that in case of heating cable failure will have no consequences on PbLi circulation;
 - the thermal behavior of pipes crossing the shield and connecting the pipe forest to TBM manifolds.





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- > Integration issues, preliminary job done but it is needed to take into account maintenance;
- The design of the cold trap has been update in order to: 1.- solve some local issues revealed by the TM analyses; 2.- allow the maintenance of the fan (only active part) without dismounting the shielding (i.e. ORE reduction);
- The changes needed to accommodate the removal of the storage tank (substituted by a small circulation tank) need to be studied more in detail. For instance, the process of filling-up the PbLi loop require the pressurization of the drainage tank since the permanent-magnets pump is not able to suck the PbLi from the tank underneath;
- From an R&D point of view also activities need to be finished so all the missing information regarding optimization (e.g. TEU) and instrumentation (e.g. T sensors) can be gathered;
- The operating conditions of the PbLi loop might also need to be adapted in the next future following ITER operating conditions.



Thank you for your attention

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Back-Up Slides

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Operating Parameters

	For each ITER Global				
	POS	TCS	STM	LTM	
PbLi Loop	NOS PbLi loop inlet pressure 0.165 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet temperature 322 °C PbLi loop outlet temperature 295 °C PbLi loop flow rate 0.65 kg/s HSOS PbLi loop inlet pressure 0.165 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet temperature 295 °C PbLi loop outlet temperature 295 °C PbLi loop flow rate 0.65 kg/s	HSOS PbLi loop inlet pressure 0.165 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet temperature 295 °C PbLi loop outlet temperature 295 °C PbLi loop flow rate 0.65 kg/s CSOS PbLi loop inlet pressure 0.165 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop outlet temperature 270°C PbLi loop outlet temperature 270°C PbLi loop flow rate 0.30 kg/s TOS PbLi loop inlet pressure 0.165 MPa PbLi loop inlet pressure 0.165 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop outlet temperature 325 °C PbLi loop outlet temperature 325 °C PbLi loop flow rate 0.65 kg/s <u>REOS</u> PbLi loop inlet pressure 0.165 MPa PbLi loop inlet pressure 0.165 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop flow rate 0.30 kg/s	LSOS PbLi loop inlet pressure 0.165 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet temperature 270°C PbLi loop outlet temperature 270°C PbLi loop flow rate 0.30 kg/s ECS PbLi loop inlet pressure 0.165 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop outlet temperature 325°C PbLi loop flow rate 0.65 kg/s EEOS PbLi loop inlet pressure 0.165 MPa PbLi loop inlet pressure 0.165 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop inlet pressure 0.078 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop outlet temperature 295°C PbLi loop outlet temperature 295°C PbLi loop flow rate 0.30 kg/s	CSOS PbLi loop inlet pressure 0.165 MPa PbLi loop outlet pressure 0.078 MPa PbLi loop inlet temperature 270 °C PbLi loop outlet temperature 270 °C PbLi loop flow rate 0.30 kg/s IDLE PbLi is drained into the storage recirculation tank. However, the loop is ready for start-up procedure. MS Loop is under maintenance with all the process fluids evacuated and stored. The loop is not ready to be restarted.	 Operational State the TBS have a set of ow Operational States defined: NOS: Normal Operatio State HSOS: Hot Stand-by Operation State CSOS: Cold Stand-by Operation State TOS: Tritium Outgassin State RFOS: Reduced Flow Operation State
		PbLi loop flow rate 0.30 kg/s			



Components Classification

Component Description	Fluid category	Safety Function	Safety Class	Location	Seismic Class	Quality Class	Tritium Class	Category PE/NPE	Design Temperature	Design Pressure
Storage Tank	Liquid (PbLi), ESP group 1, Gas (Helium), ESP group 2	Confinement	SIC-2	11-L1-C16	SC1(SF)	QC1	TC 2A	IV / N2	350	10.9
Pump	Liquid (PbLi), ESP group 1	Confinement	SIC-2	11-L1-C16	SC1(S)	QC1	TC 2A	II / N2	350	10.9
Cold trap	Liquid (PbLi), ESP group 1	Confinement	SIC-2	11-L1-C16	SC1(SF)	QC1	TC 2A	II / N2	350	10.9
TEU	Liquid (PbLi), ESP group 1	Confinement	SIC-2	11-L1-C16	SC1(SF)	QC1	TC 2A	II / N2	500	10.9
Heat Exchanger (Cooler)	Liquid (PbLi), ESP group 1	Confinement	SIC-2	11-L1-C16	SC1(S)	QC1	TC 2A	II / N2	500	10.9
Heater	Liquid (PbLi), ESP group 1	Confinement	SIC-2	11-L1-C16	SC1(S)	QC1	TC 2A	SEP/N2	500	10.9
Relieftank	Gas (water), ESP group 2, Liquid (PbLi), ESP group 1	Confinement	SIC-2	11-L1-C16	SC1(S)	QC1	TC 2A	IV / N2	500	10.9
Safety Isolation Valves	Liquid (PbLi), ESP group 1	Confinement	SIC-1	11-L1-C16	SC1(SF)	QC1	TC 2A	IV / N2	500	10.9

The maximum classification for the PbLi loop is PED Category IV and ESPN Level N2 -> Maximum in ITER

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Dose rate in PC #16



Pipe insulation and shielding removed for visual purposes

Dose rate in PC #16



Image courtesy of NIER Ingegneria

